



CECAM International Summer School

Hot topic 4

First-principles based catalytic reaction engineering

Matteo Maestri

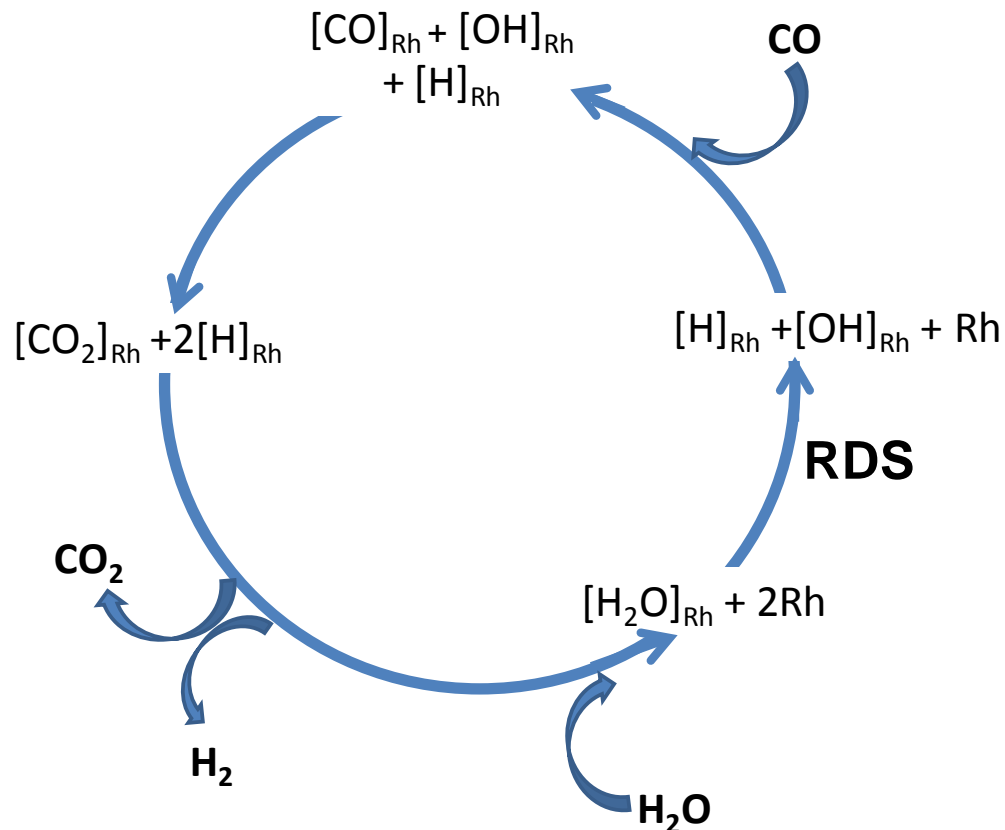


July 23, 2013

Conversationshaus - Norderney, Germany

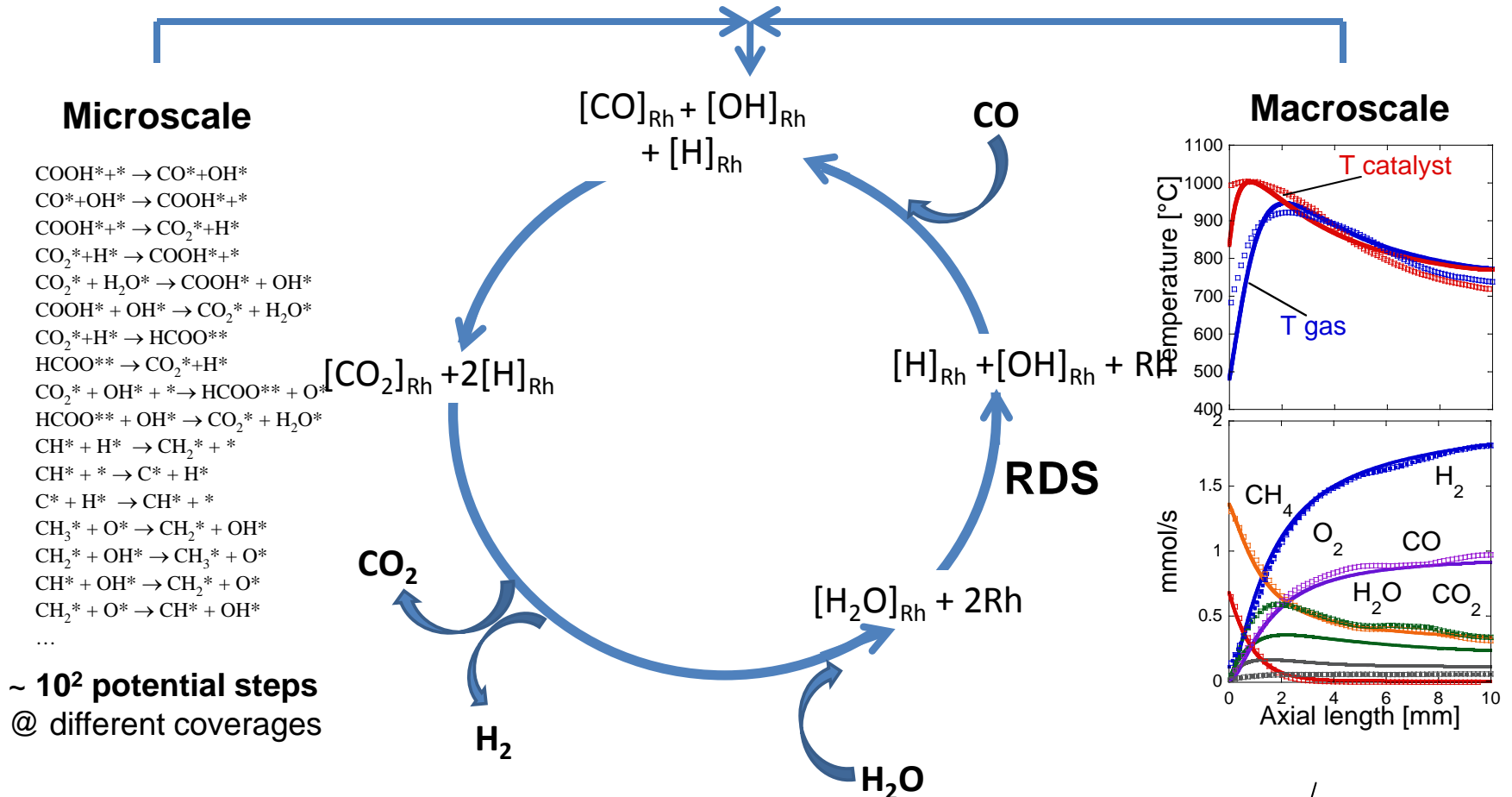
Catalytic cycle

Consists of the elementary steps through which the reactants convert to the products

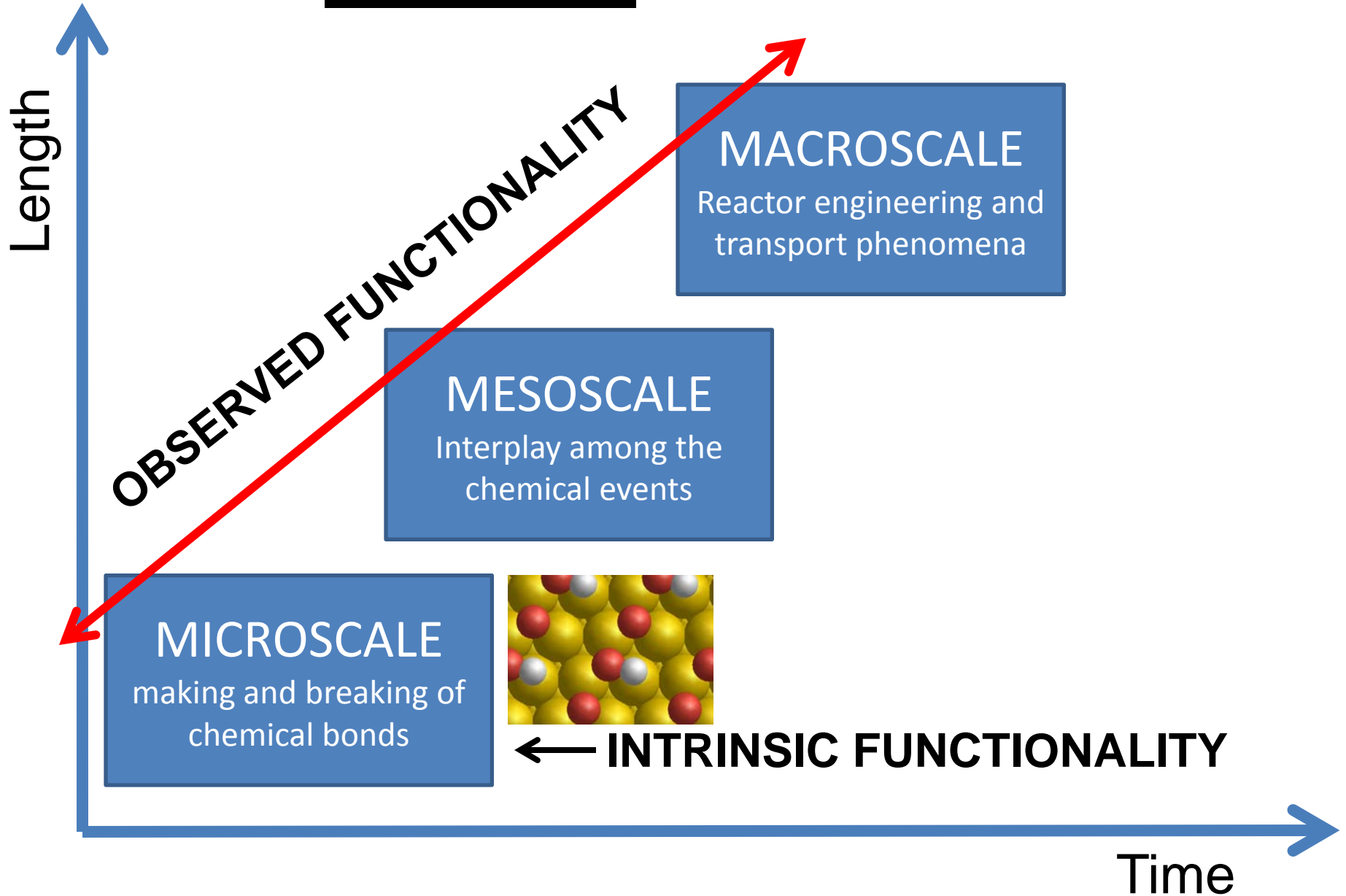


“*E pluribus unum*”

Result of the interplay among phenomena at different scales



Need of bridging between the scales





Frontiers in Reactor Engineering
Milorad P. Dudukovic
Science **325**, 698 (2009);
DOI: 10.1126/science.1174274

PERSPECTIVE

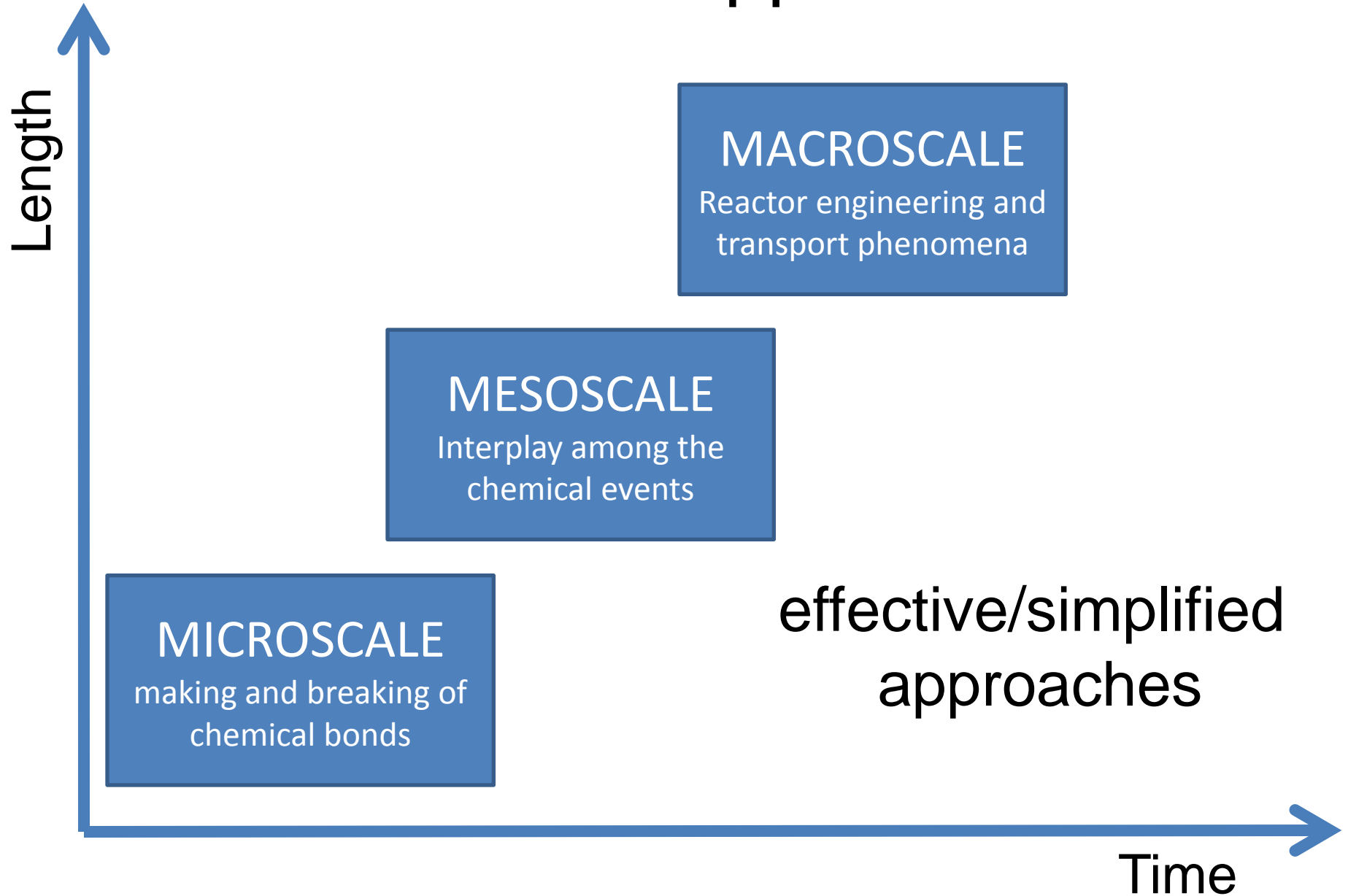
Frontiers in Reactor Engineering

Milorad P. Dudukovic

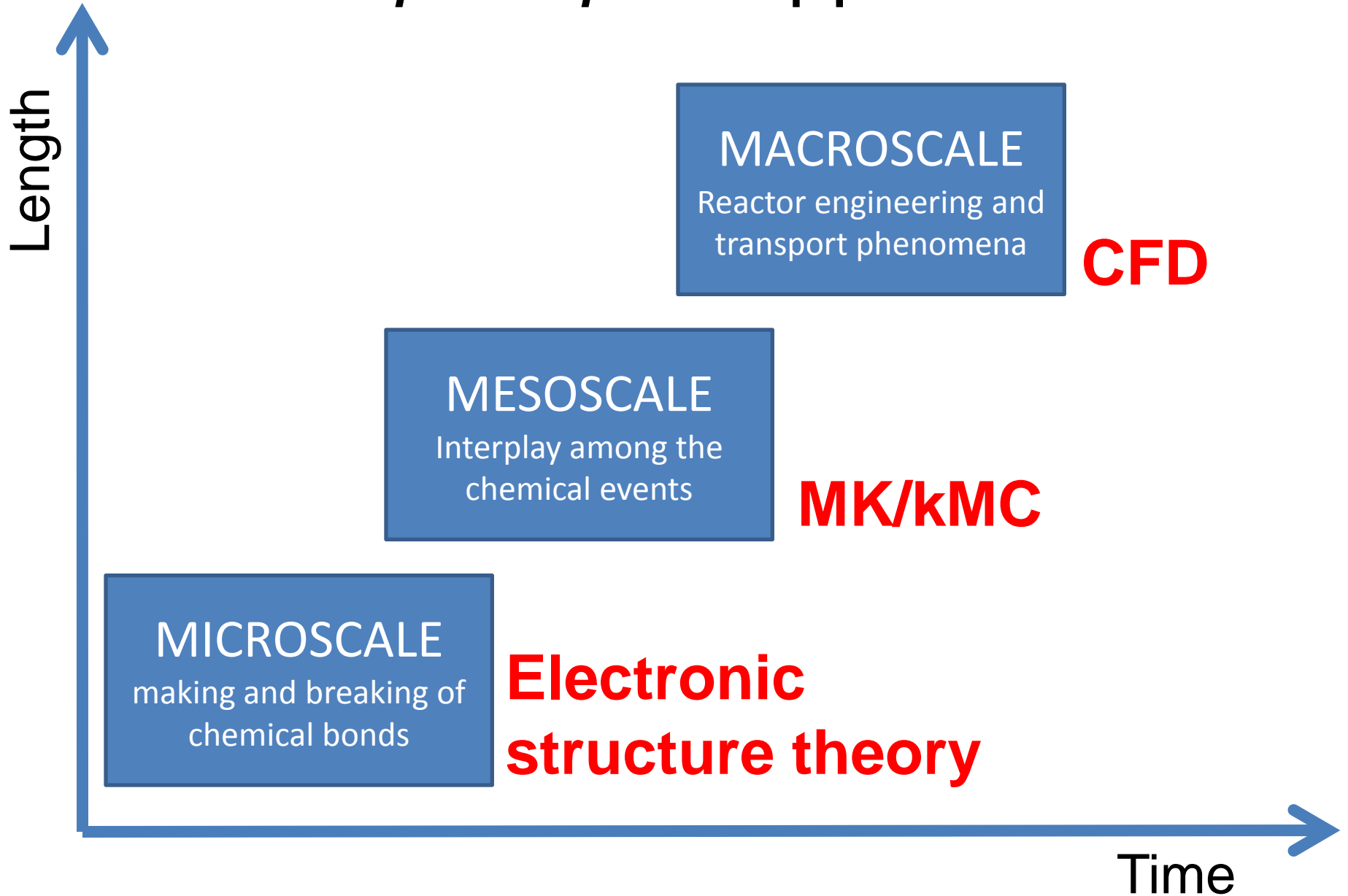
The key challenge for reactor engineering is to establish **the scientifically based sustainable technologies** necessary for meeting the future energy, environmental, and materials needs of the world. This goal requires **advancing our scientific understanding of multiscale kinetic transport interactions** to enable better reactor choice and to ensure higher reactor and process efficiencies.

Our current increased awareness of the finiteness of our resources raises the bar for future reactor technology. Instead of continuing the application of principles at the rudimentary level, the main task now is to provide **an improved scientific basis** for conducting chemical transformations in an environmentally acceptable, energy-efficient, and sustainable manner.

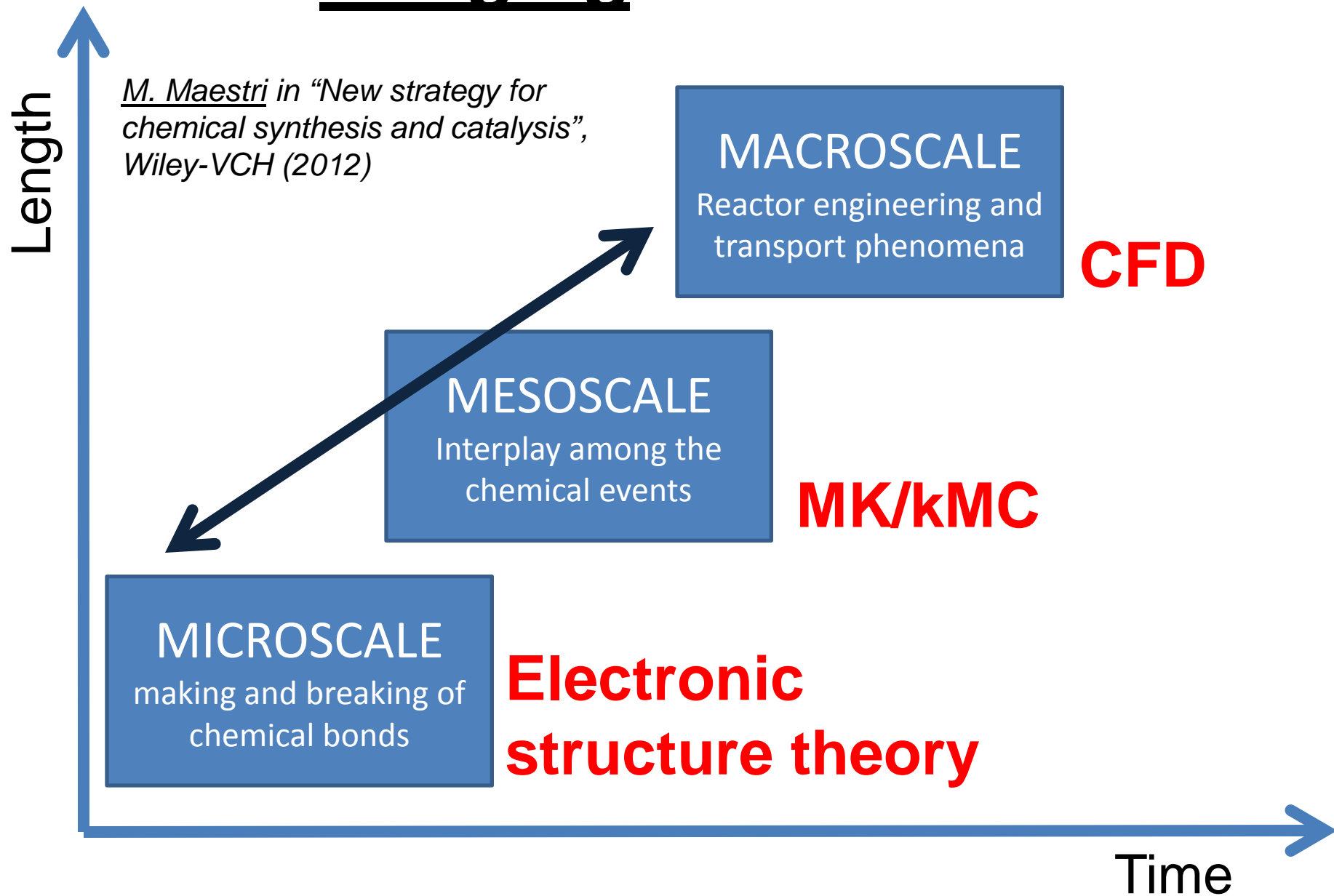
From a “traditional” approach to CRE...



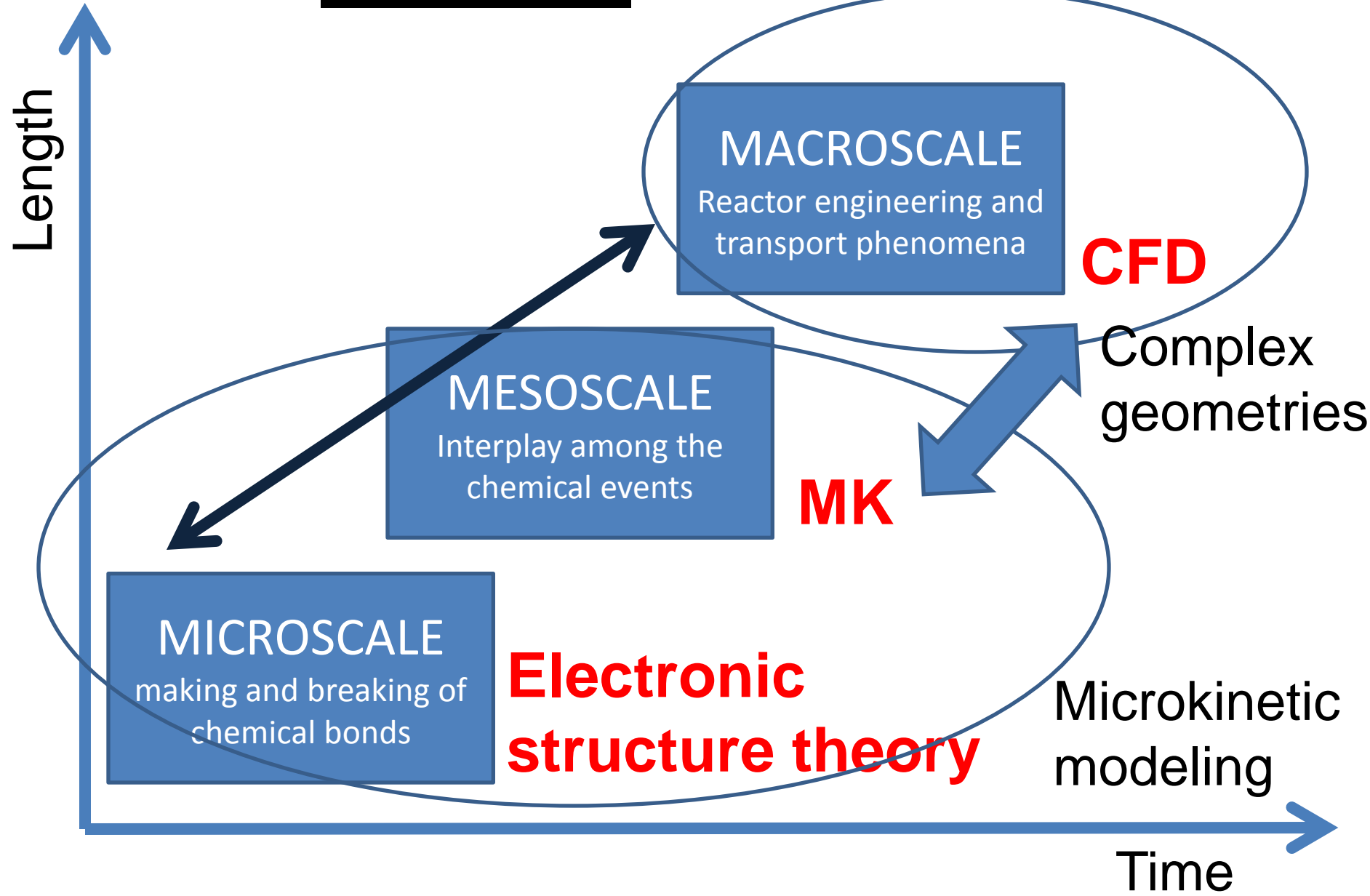
...to a *first-principles* approach to CRE



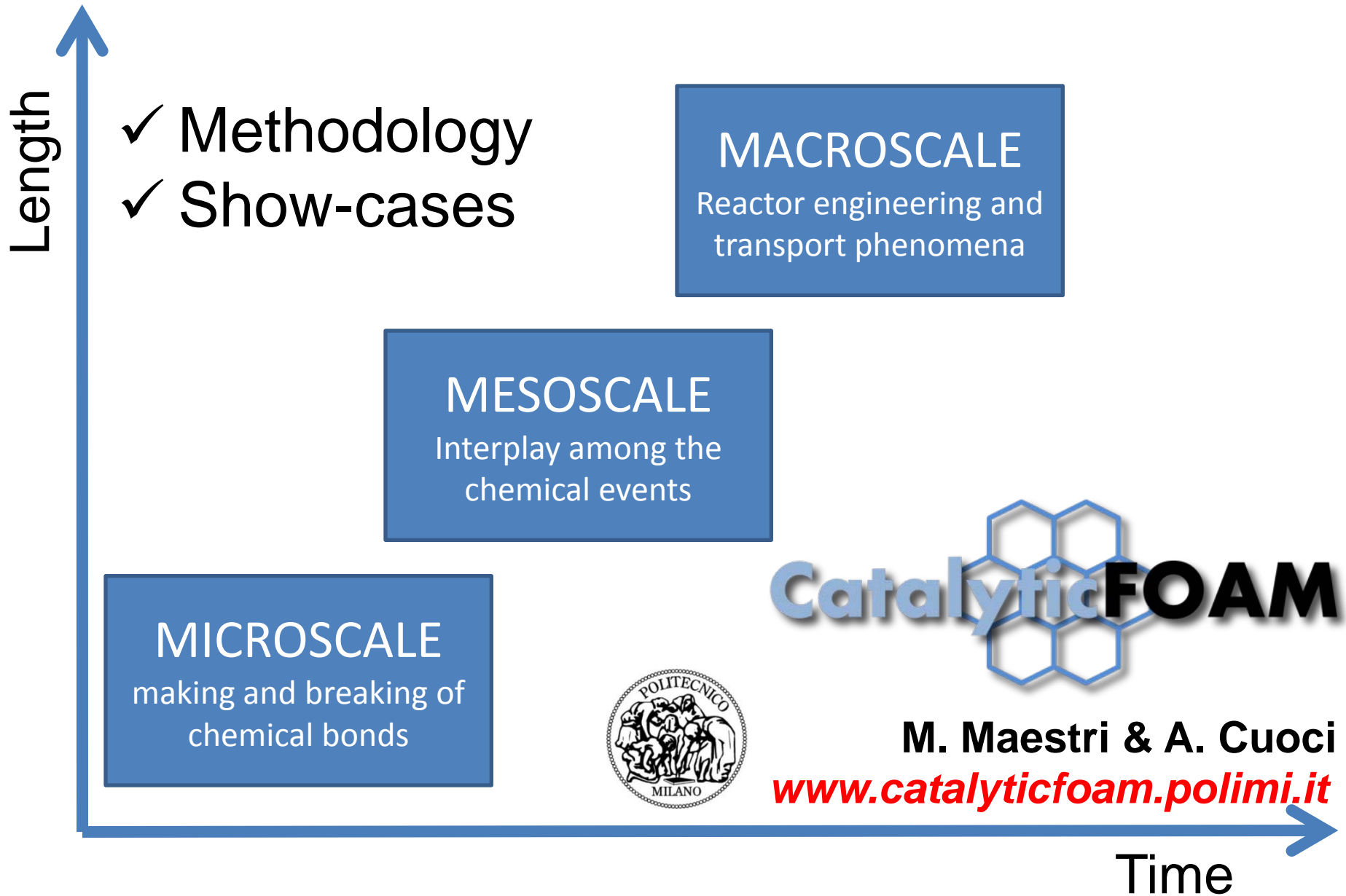
Need of “bridging” between the scales



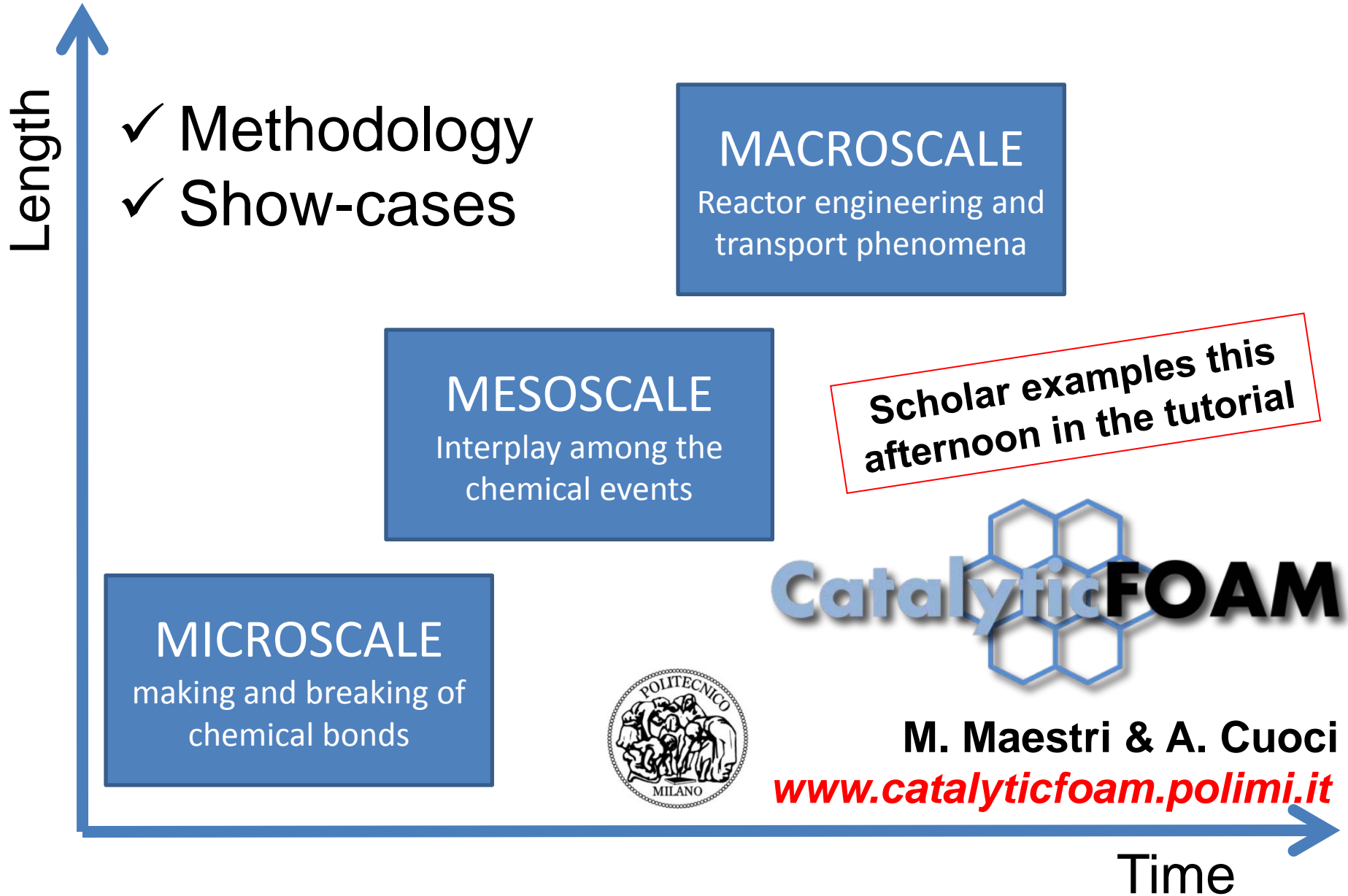
Need of “bridging” between the scales



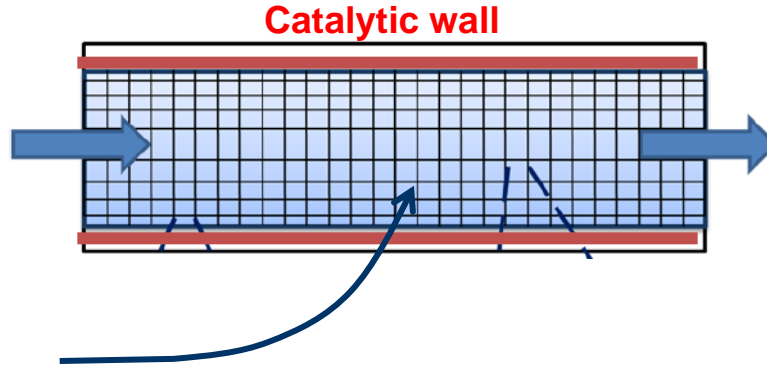
Outline



Outline



Governing equations



$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0$$

continuity

$$\frac{\partial}{\partial t}(\rho \mathbf{v}) + \nabla \cdot (\rho \mathbf{v} \mathbf{v}) = -\nabla p + \nabla \cdot \left[\mu (\nabla \mathbf{v} + \nabla \mathbf{v}^T) - \frac{2}{3} \mu (\nabla \mathbf{v}) \mathbf{I} \right] + \rho \mathbf{g}$$

momentum

$$\frac{\partial}{\partial t}(\rho \omega_k) + \nabla \cdot (\rho \omega_k \mathbf{v}) = -\nabla \cdot (\rho \omega_k \mathbf{V}_k) + \dot{\Omega}_k^{\text{hom}} \quad k = 1, \dots, NG$$

mass

$$\rho \hat{C}_P \frac{\partial T}{\partial t} + \rho \hat{C}_P \mathbf{v} \nabla T = \nabla \cdot (\lambda \nabla T) - \rho \sum_{k=1}^{NG} \hat{C}_{P,k} \omega_k \mathbf{V}_k - \sum_{k=1}^{NG} \hat{H}_k^{\text{hom}} \dot{\Omega}_k^{\text{hom}}$$

energy

Governing equations

Non-catalytic walls

$$\nabla \omega_k \Big|_{inert} = 0$$

$$T \Big|_{inert} = f(t, T)$$

$$\nabla T \Big|_{inert} = g(t, T)$$

Catalytic walls

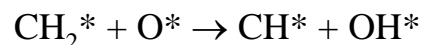
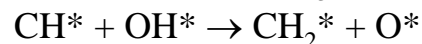
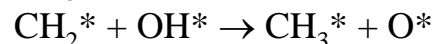
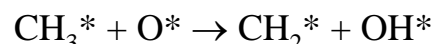
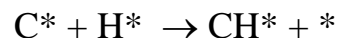
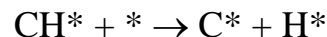
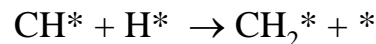
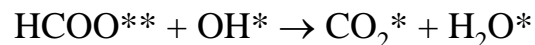
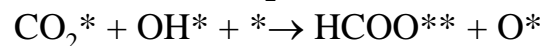
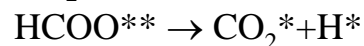
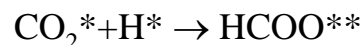
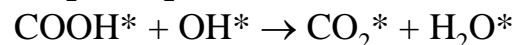
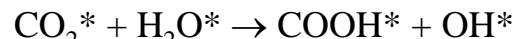
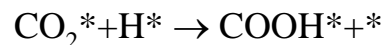
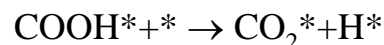
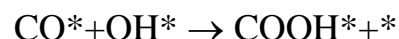
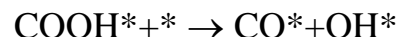
$$\rho \Gamma_{k,mix} (\nabla \omega_k) \Big|_{catalytic} = -\alpha_{cat} \dot{\Omega}_k^{het} \quad k = 1, \dots, NG$$

$$\lambda (\nabla T) \Big|_{catalytic} = -\alpha_{cat} \sum_{j=1}^{NR} \Delta H_j^{het} \dot{r}_j^{het}$$

$$\sigma_{cat} \frac{\partial \theta_i}{\partial t} = \dot{\Omega}_i^{het} \quad i = 1, \dots, NS$$

Adsorbed (surface) species

Detailed microkinetic models



...

$$r_j = A_j \cdot T^{\beta_j} \cdot \exp\left(-\frac{E_{att,j}(\theta_i)}{RT}\right) \prod_{i=1}^{NC} (c_i)^{\nu_{ij}}$$

Numerical challenges

✓ Dimensions of the system

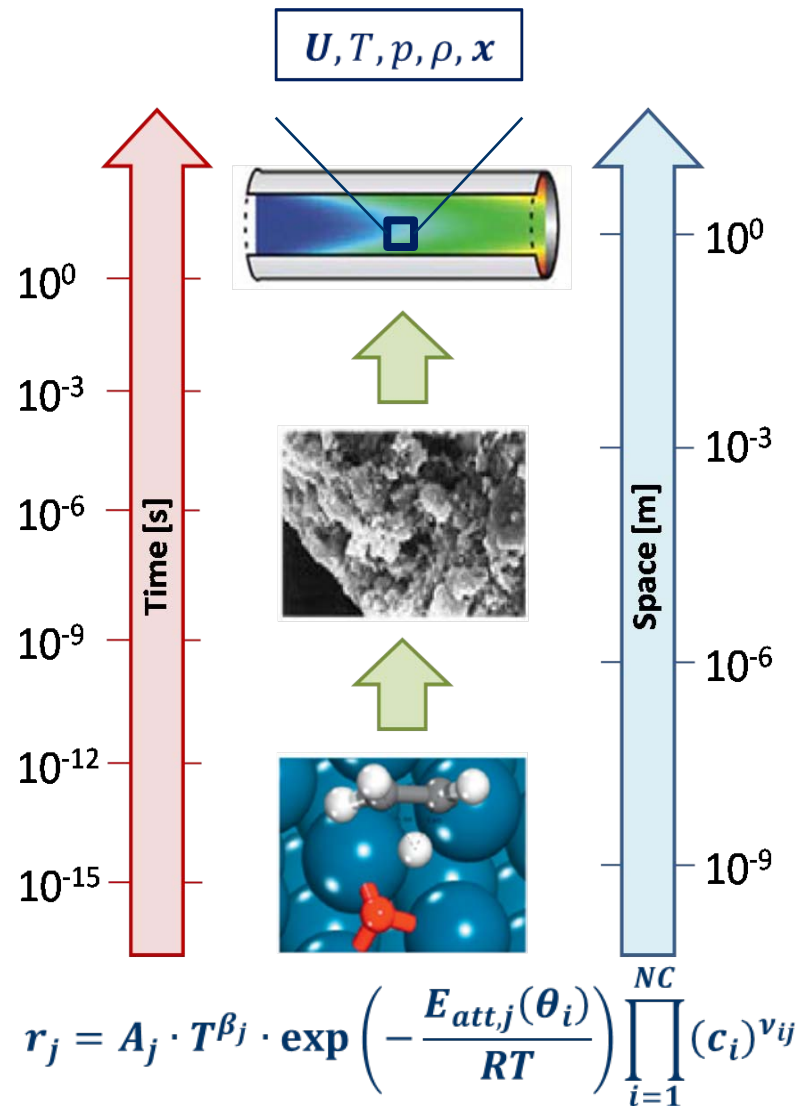
- Proportional to the number of species
- Proportional to the number of cells

✓ Stiffness

- Different temporal scales involved
- Different spatial scales involved

✓ Non-linearity

- Source term non linear in concentrations and temperature
- Coverage dependence of activation energy

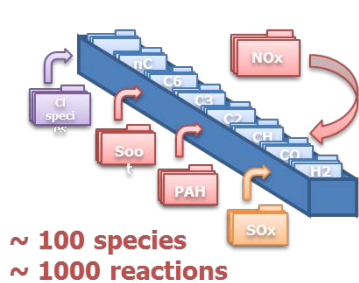


Numerical solution

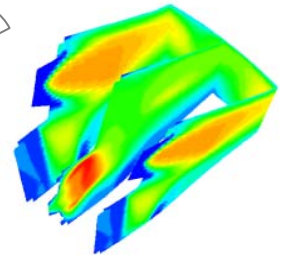
Fully segregated algorithms

- 😊 easy to implement and computationally efficient
- ☹️ unfeasible when large, stiff kinetic mechanisms are used

Detailed kinetic schemes



Complex geometries



Strong non linearity of reaction terms
High stiffness

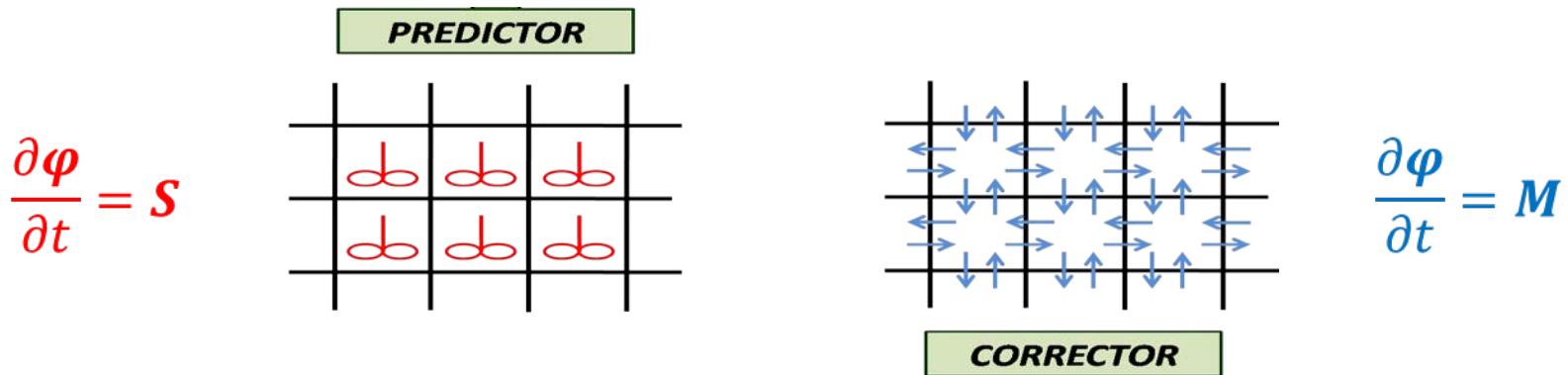
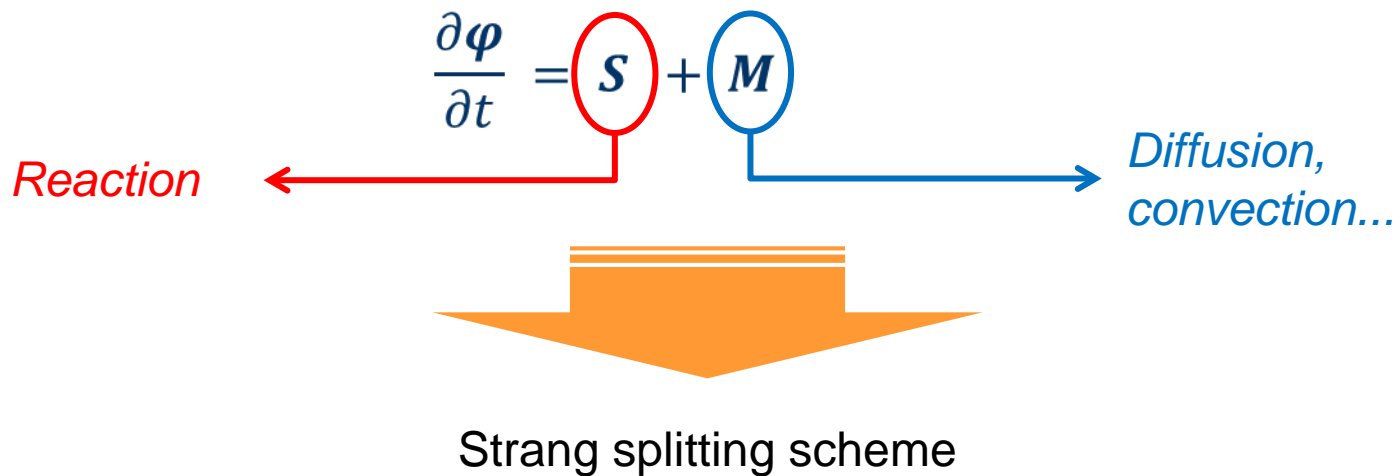
Fully coupled algorithms

- 😊 all the processes and their interactions are considered simultaneously
- 😊 natural way to treat problems with multiple stiff processes
- ☹️ the resulting system of equations can be extremely large and the computational cost prohibitive

Operator-splitting methods

- 😊 usually avoid many costly matrix operations
- 😊 allow the best numerical method to be used for each type of term or process
- ☹️ the resulting algorithms can be very complex and usually differ from term to term

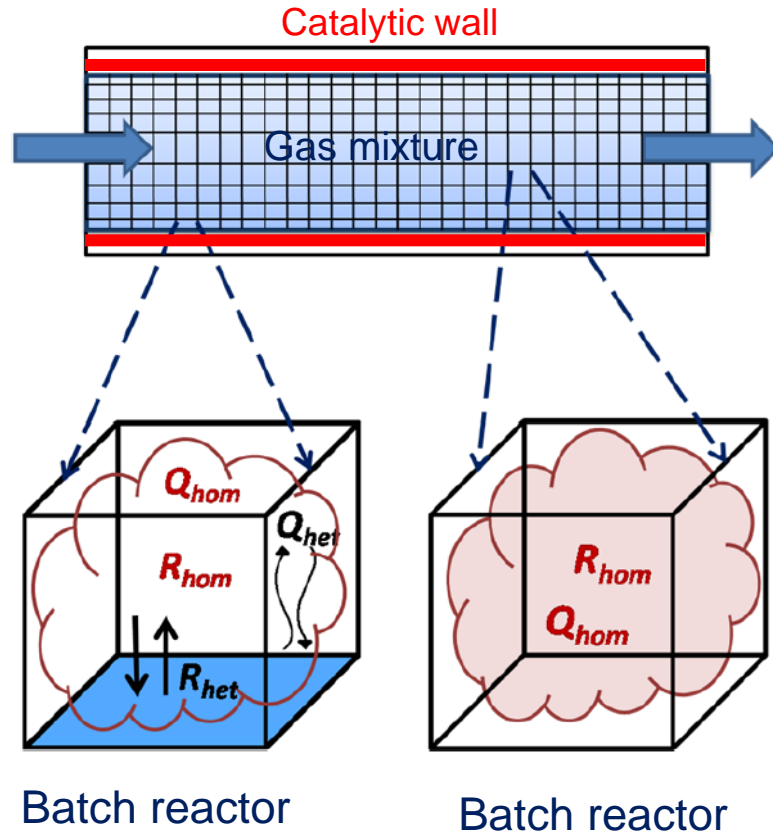
Operator-splitting algorithm



Z. Ren, S. B. Pope, *Journal of Computational Physics*, 2008

M. Maestri, A. Cuoci, *Chemical Engineering Science*, 96 (2013) 106-117

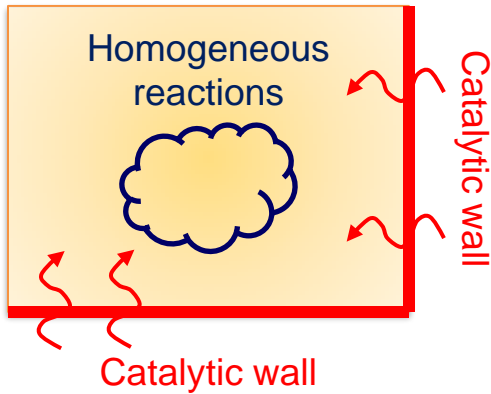
Reactor network



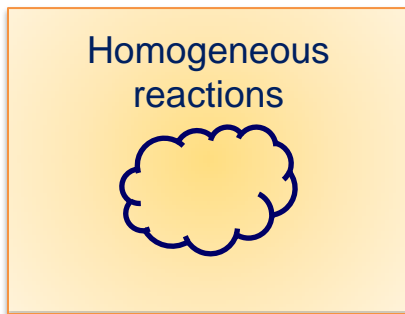
Each computational cell behaves as a chemical reactor in the splitting-operator algorithm (chemical step)

Each reactor is described by a set of stiff ODE, which must be integrated on the time step Δt

Reactor network

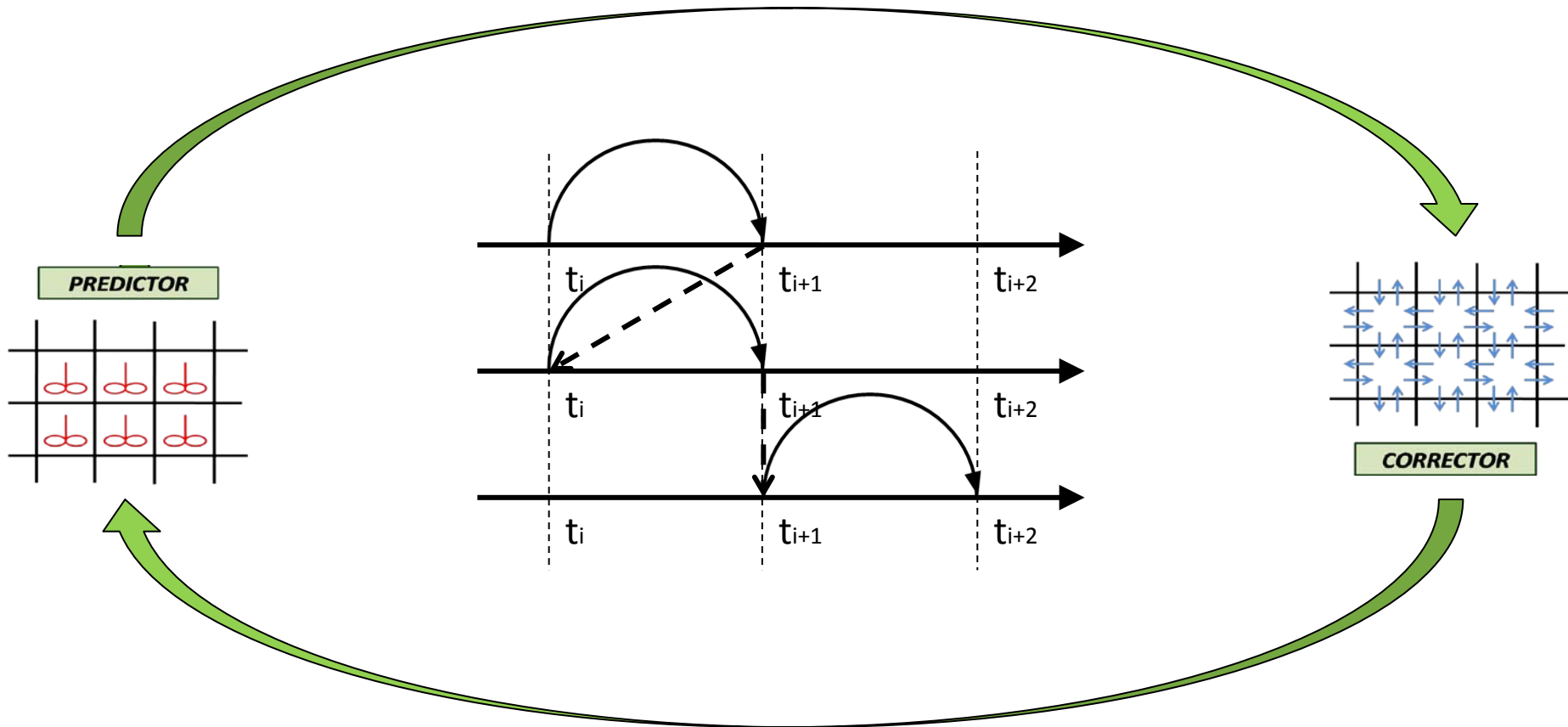


$$\left\{ \begin{array}{l} \rho \frac{d\omega_k}{dt} = \dot{\Omega}_k^{\text{hom}} + \frac{1}{V} \left\{ \sum_{j=1}^{NF} \alpha_j^{\text{cat}} A_j \dot{\Omega}_{k,j}^{\text{het}} - \omega_k \sum_{j=1}^{NF} \left[\alpha_j^{\text{cat}} A_j \sum_{k=1}^{NG} \dot{\Omega}_{k,j}^{\text{het}} \right] \right\} \quad k=1, NG \\ \rho \hat{C}_P \frac{dT}{dt} = - \sum_{k=1}^{NG} \hat{H}_k^{\text{hom}} \Omega_k^{\text{hom}} + \frac{1}{V} \sum_{j=1}^{NF} \alpha_j^{\text{cat}} A_j \sum_{k=1}^{NG} \dot{\Omega}_{k,j}^{\text{het}} (\hat{H}_{k,j}^{\text{het}} - \hat{H}_k^{\text{hom}}) \\ \sigma_{\text{cat}} \frac{\partial \theta_{i,j}}{\partial t} = \dot{\Omega}_{i,j}^{\text{het}} \quad i=1, \dots, NS \quad j=1, \dots, NF \end{array} \right.$$



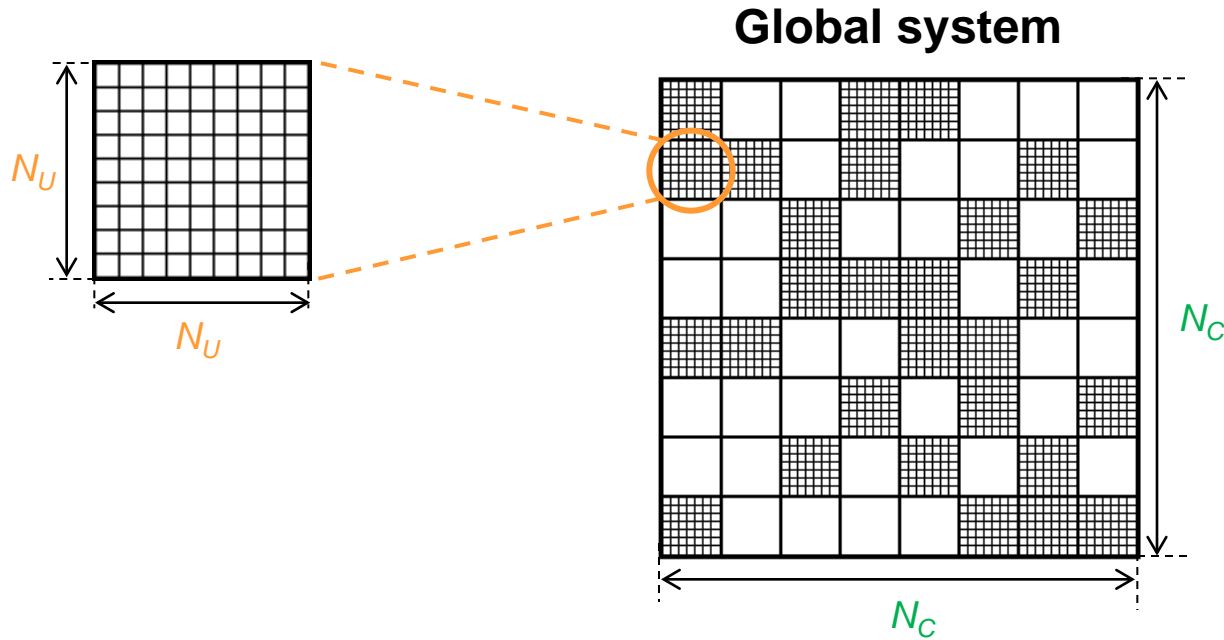
$$\left\{ \begin{array}{l} \rho \frac{d\omega_k}{dt} = \dot{\Omega}_k^{\text{hom}} + \frac{1}{V} \left\{ \sum_{j=1}^{NF} \alpha_j^{\text{cat}} A_j \dot{\Omega}_{k,j}^{\text{het}} - \omega_k \sum_{j=1}^{NF} \left[\alpha_j^{\text{cat}} A_j \sum_{k=1}^{NG} \dot{\Omega}_{k,j}^{\text{het}} \right] \right\} \quad k=1, NG \\ \rho \hat{C}_P \frac{dT}{dt} = - \sum_{k=1}^{NG} \hat{H}_k^{\text{hom}} \Omega_k^{\text{hom}} + \frac{1}{V} \sum_{j=1}^{NF} \alpha_j^{\text{cat}} A_j \sum_{k=1}^{NG} \dot{\Omega}_{k,j}^{\text{het}} (\hat{H}_{k,j}^{\text{het}} - \hat{H}_k^{\text{hom}}) \\ \sigma_{\text{cat}} \frac{\partial \theta_{i,j}}{\partial t} = \dot{\Omega}_{i,j}^{\text{het}} \quad i=1, \dots, NS \quad j=1, \dots, NF \end{array} \right.$$

Operator-splitting algorithm



The procedure is iterated on the next time step

Jacobian matrix



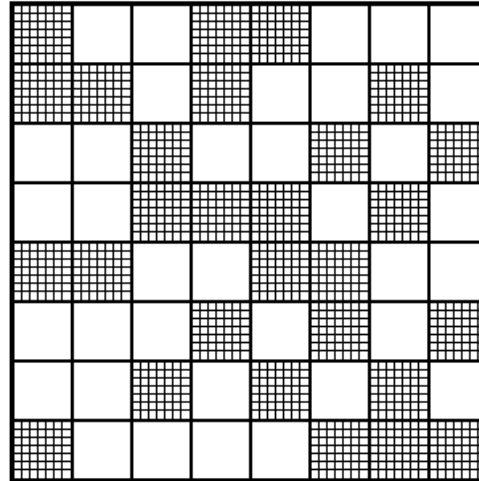
$$\frac{\partial \varphi}{\partial t} = M + S$$

Jacobian matrix:

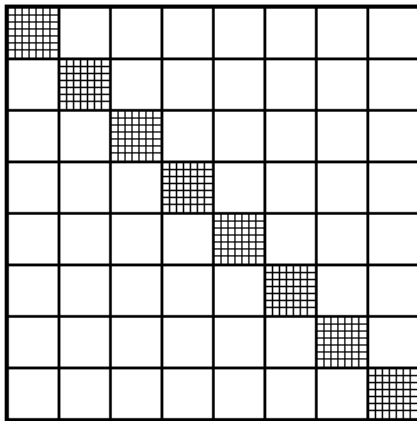
- ✓ Sparse
- ✓ Unstructured
- ✓ Blocks

Source term

Global system



Source term



$$\frac{\partial \varphi}{\partial t} = M + S$$

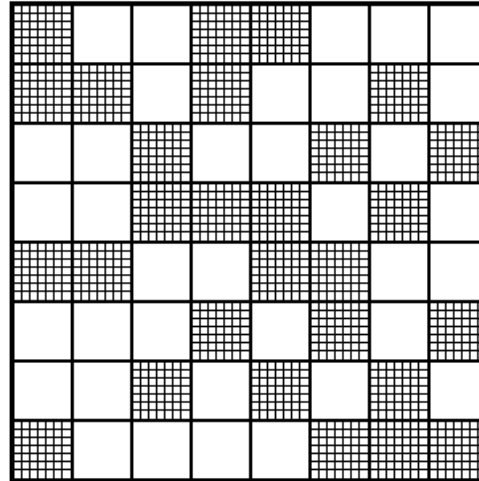
Jacobian matrix:

- ✓ Sparse
- ✓ Diagonal

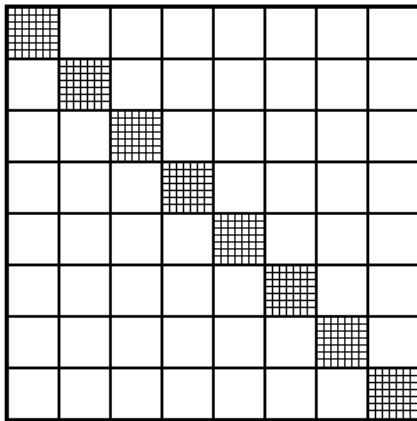
$$\frac{\partial \varphi}{\partial t} = S$$

Transport term

Global system



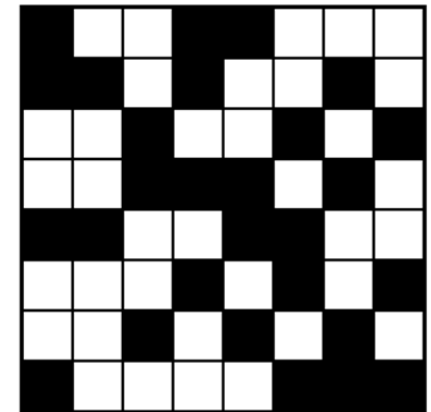
Source term



$$\frac{\partial \phi}{\partial t} = S$$



Transport term



$$\frac{\partial \phi}{\partial t} = M$$

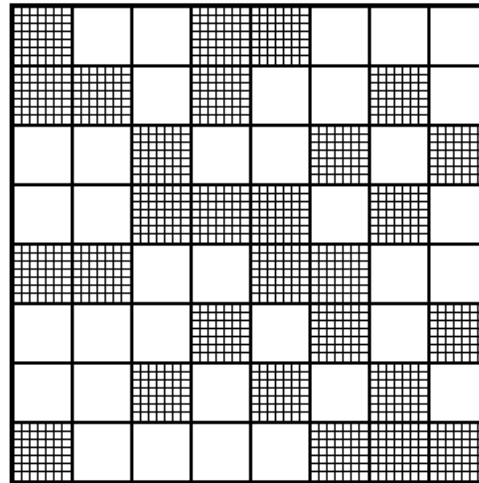
$$\frac{\partial \phi}{\partial t} = M + S$$

Jacobian matrix:

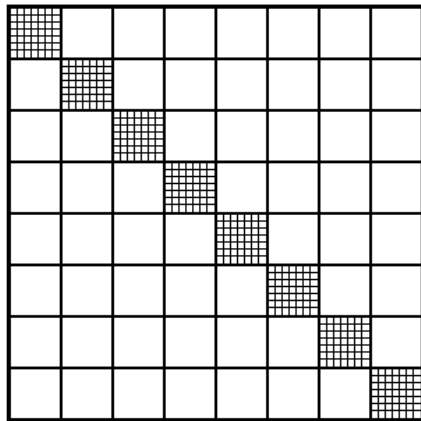
- ✓ Sparse
- ✓ Unstructured

Operator-splitting algorithm

Global system



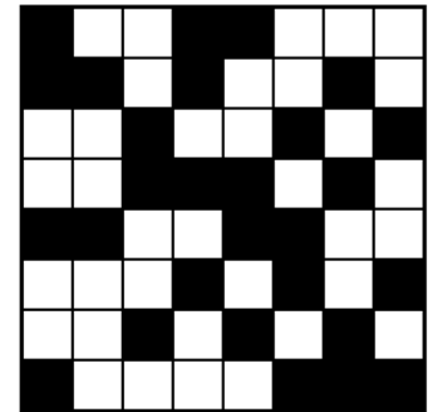
Source term



$$\frac{\partial \phi}{\partial t} = S$$



Transport term

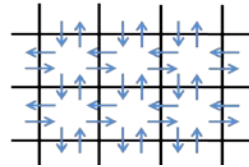
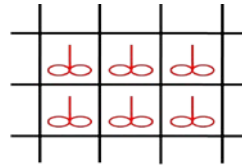
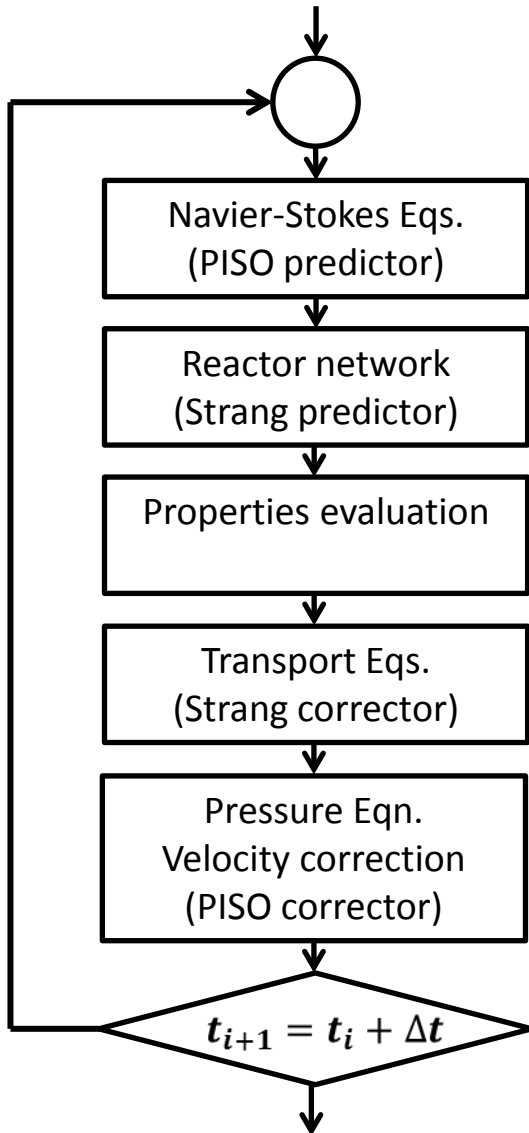


$$\frac{\partial \phi}{\partial t} = M$$

$$\frac{\partial \phi}{\partial t} = M + S$$

Use of a suitable algorithm for each sub-problem

Solution procedure

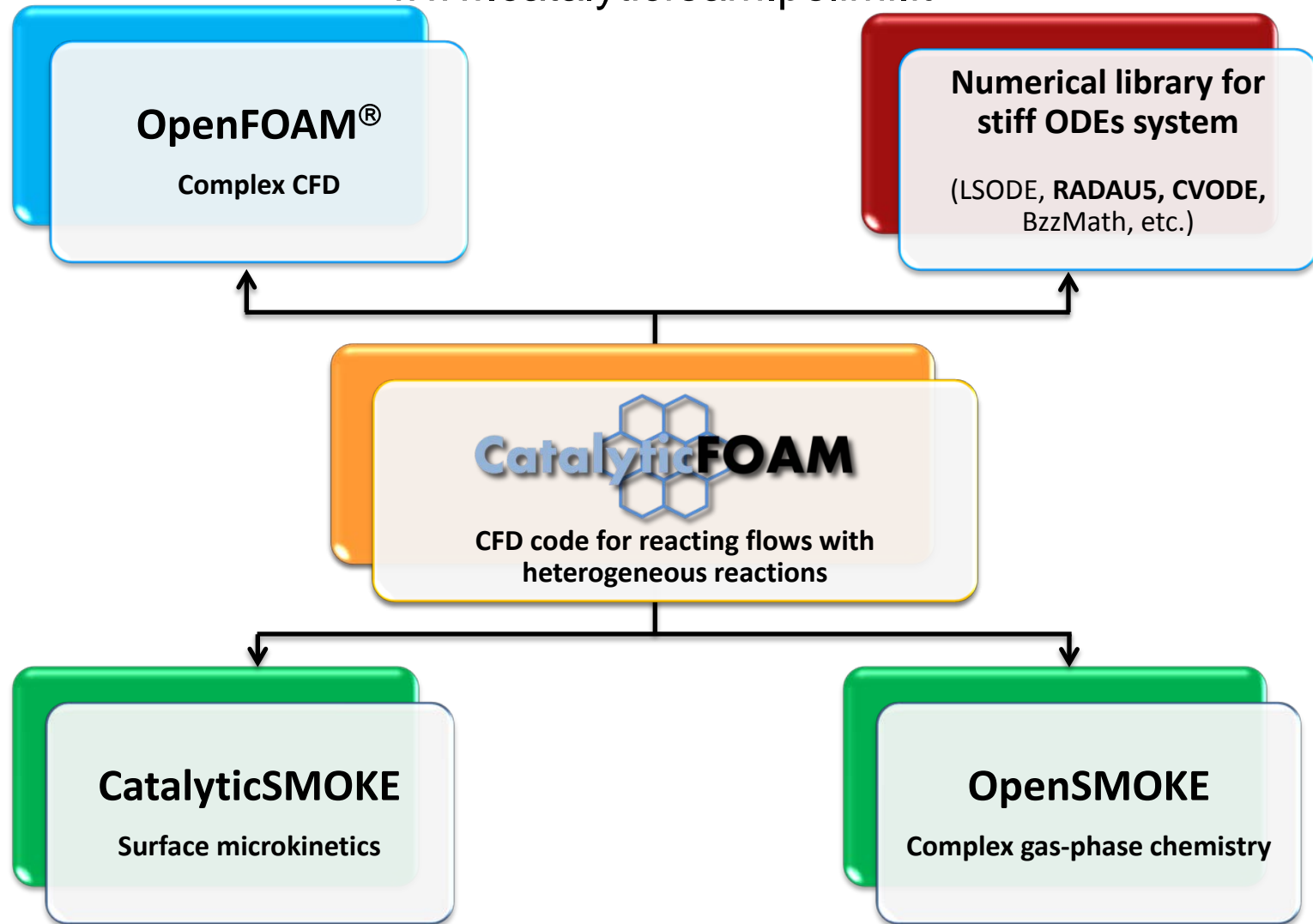


Main features:

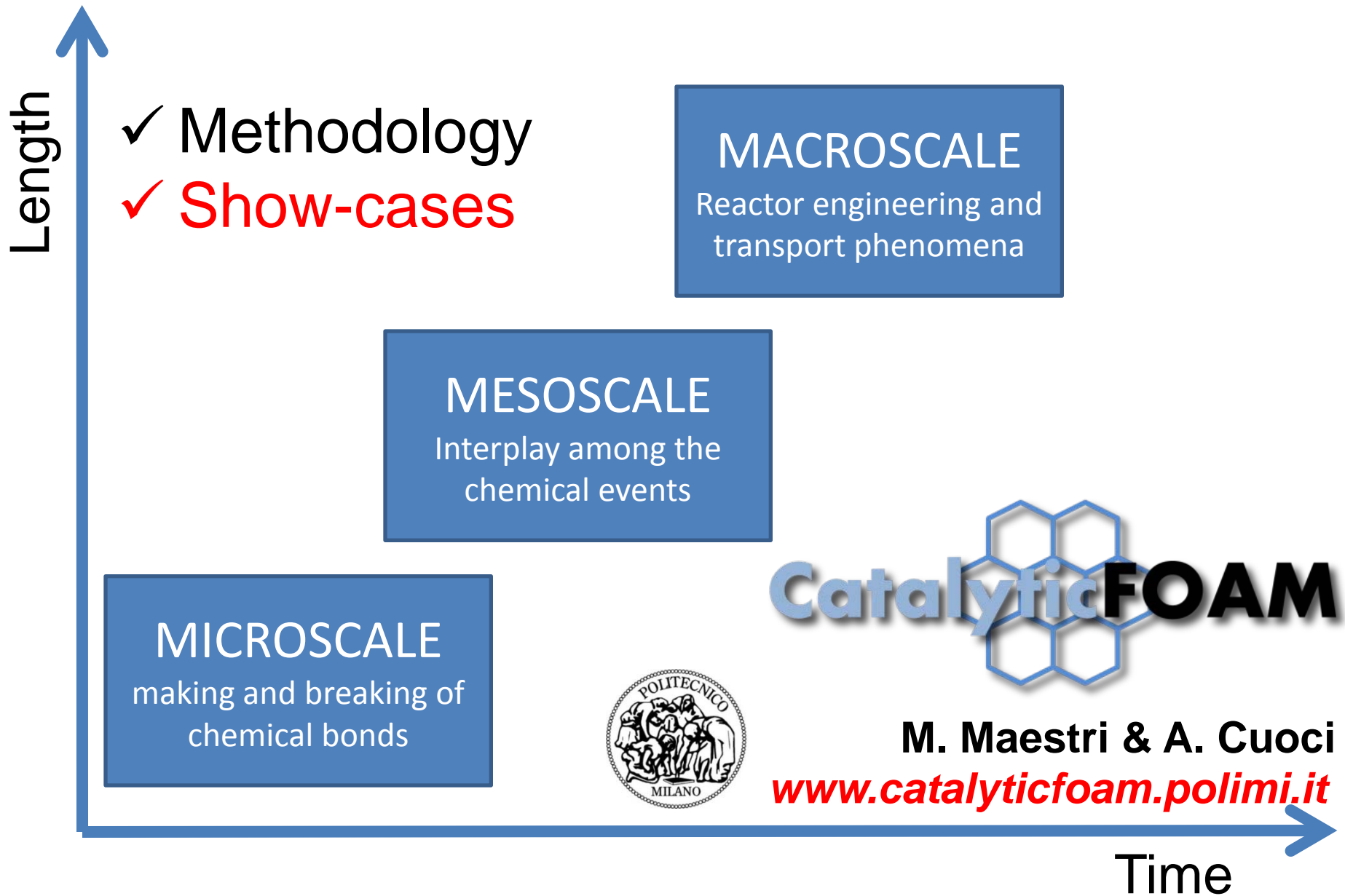
- ✓ Solution of the Navier-Stokes equations (laminar and turbulent regime)
- ✓ No limit to the number of species and reactions
- ✓ No limit in geometry

catalyticFOAM structure

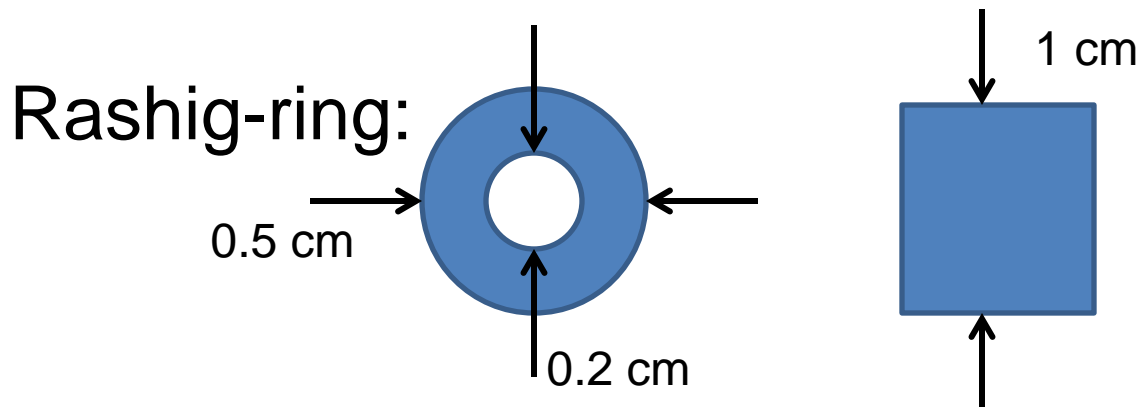
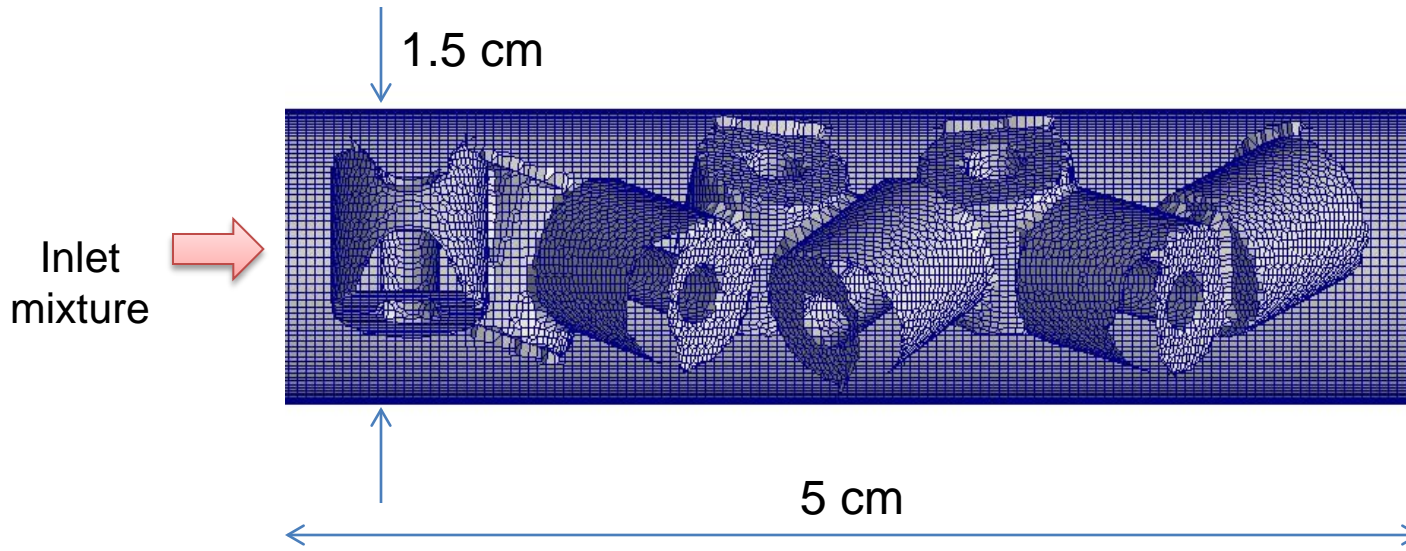
www.catalyticfoam.polimi.it



Outline



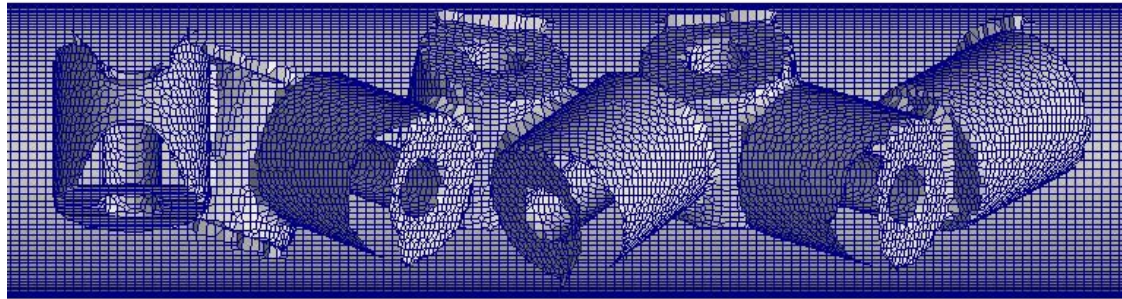
Show-case I: Rashig-ring bed



Show-case I: Rashig-ring bed

Laminar flow ($Re = 50$)

Inlet
mixture



Operating conditions	
Internal diameter	1.5 cm
Total length	5 cm
H ₂ mole fraction	0.04 (-)
O ₂ mole fraction	0.01 (-)
N ₂ mole fraction	0.95 (-)
Temperature	473.15 K
Inlet velocity	0.2 m/s

C1 microkinetic model on Rh:

82 reaction steps

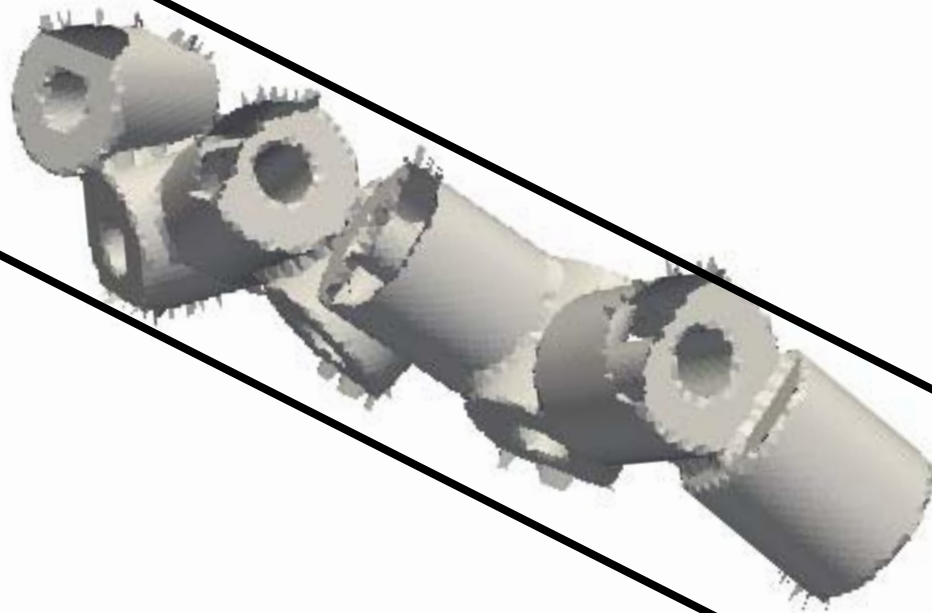
13 adsorbed species

UBI-QEP and DFT refinement

M. Maestri et al., AIChE J., 2009

Show-case I: Rashig-ring bed

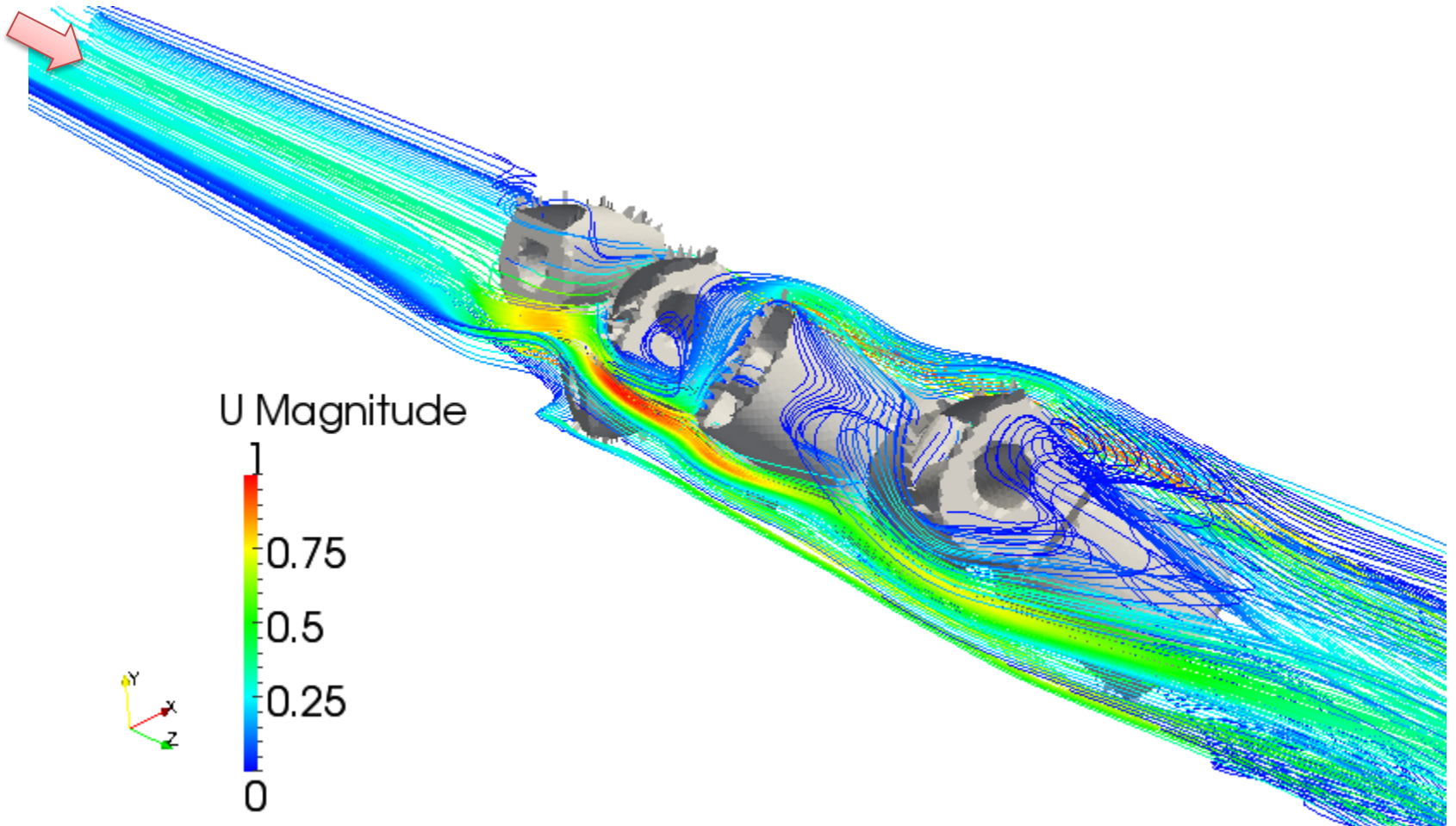
Inlet mixture



Show-case I: Rashig-ring bed

Flow-field

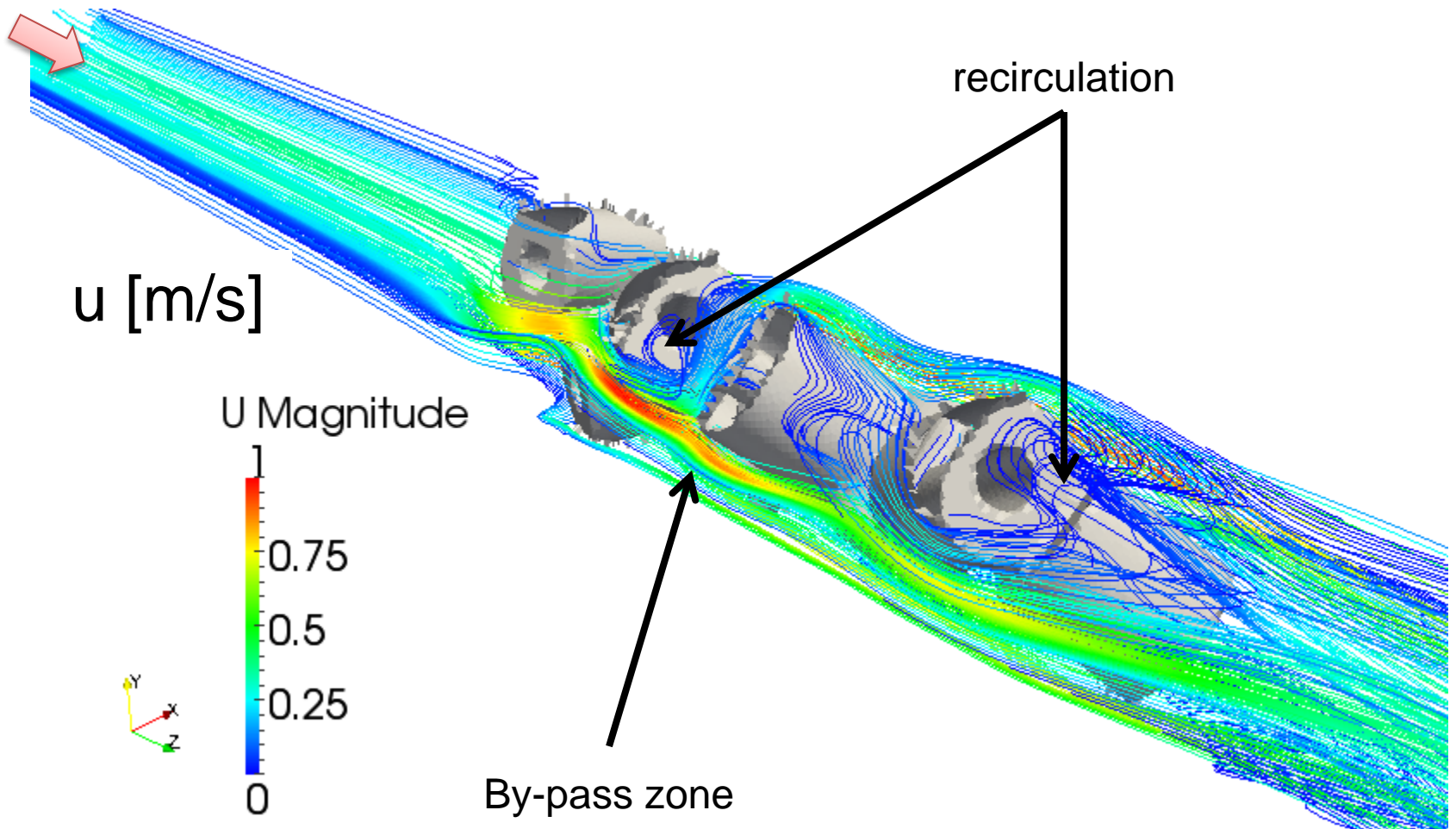
Inlet mixture



Show-case I: Rashig-ring bed

Flow-field

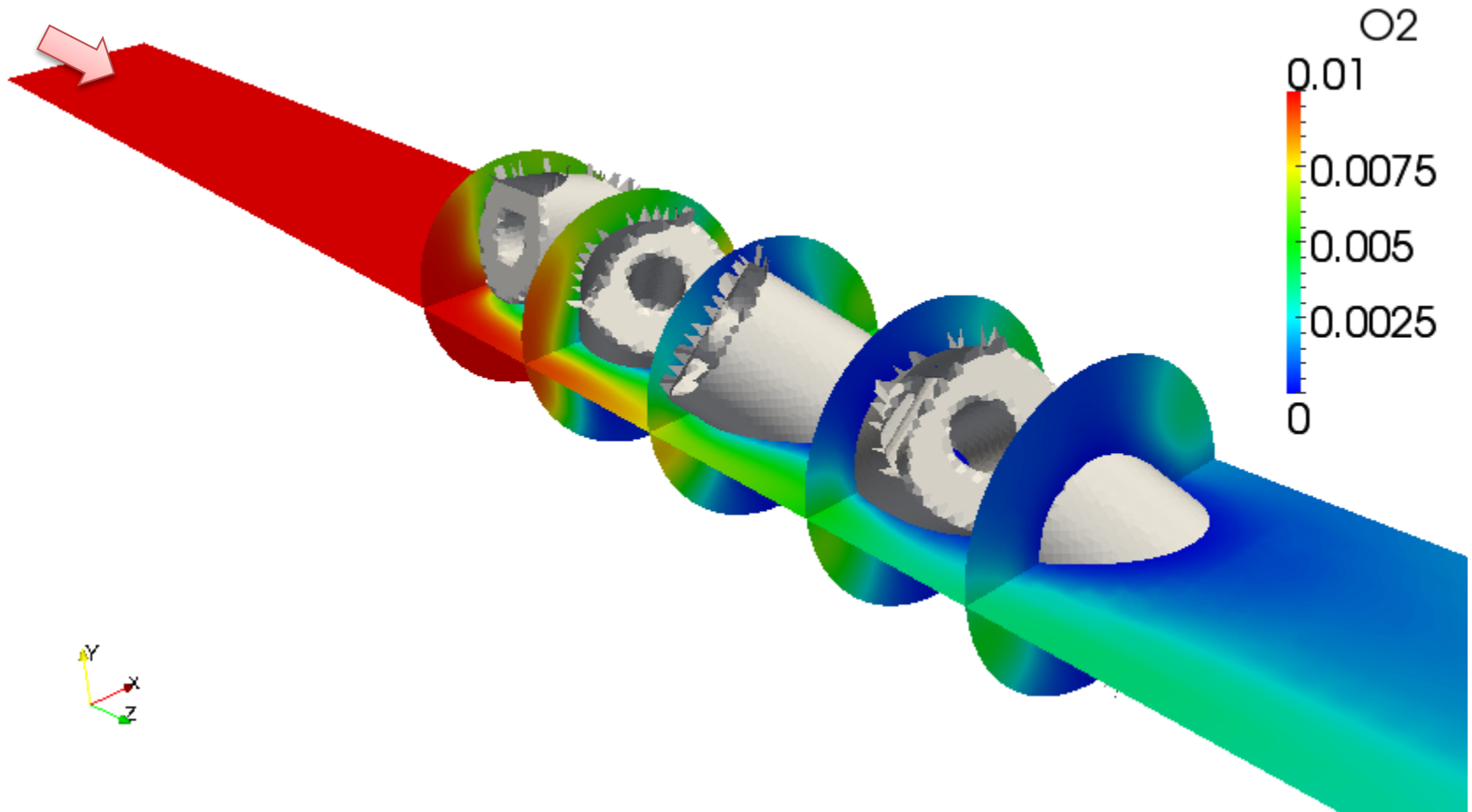
Inlet mixture



Show-case I: Rashig-ring bed

Gas-phase species

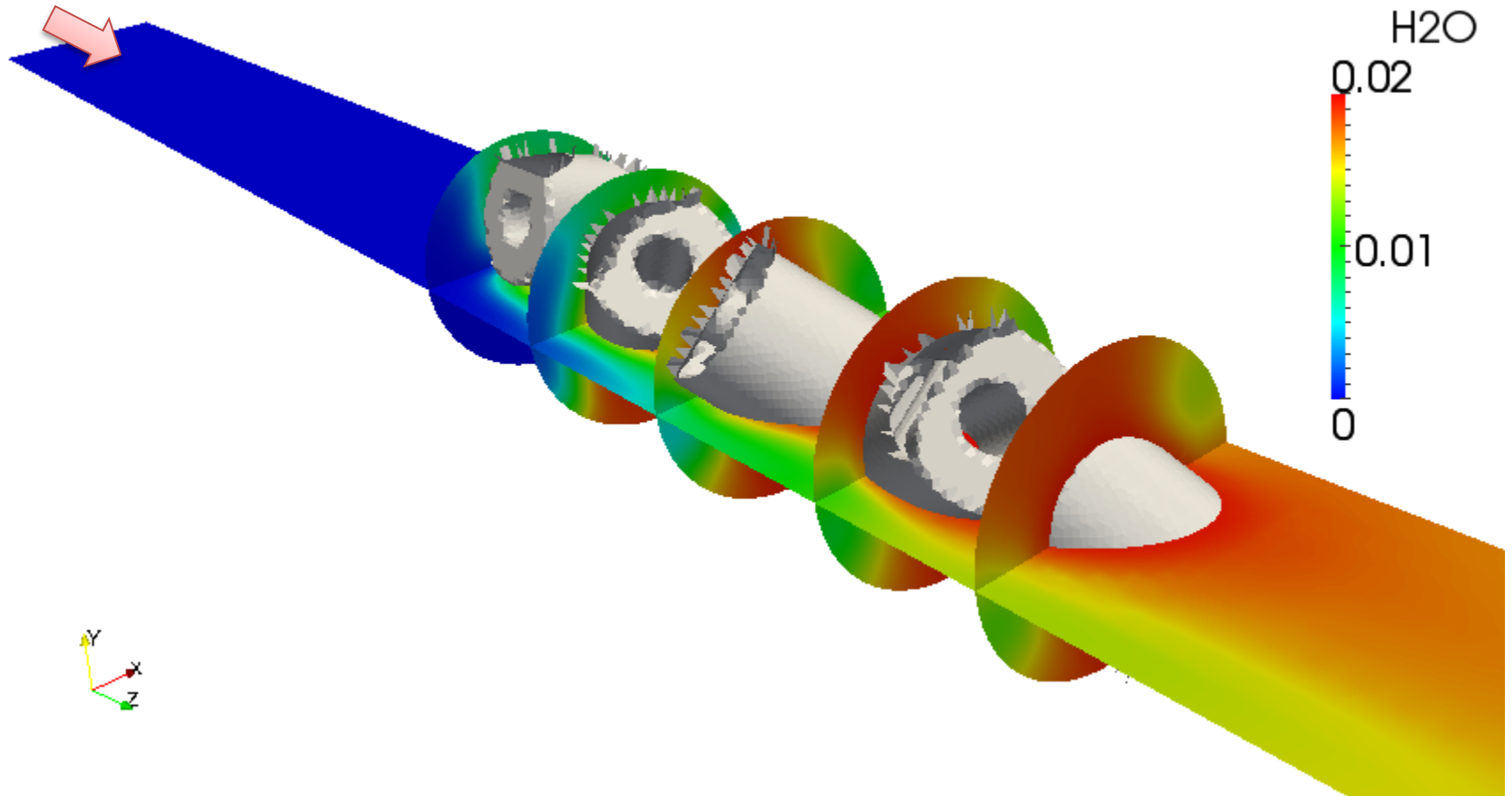
Inlet mixture



Show-case I: Rashig-ring bed

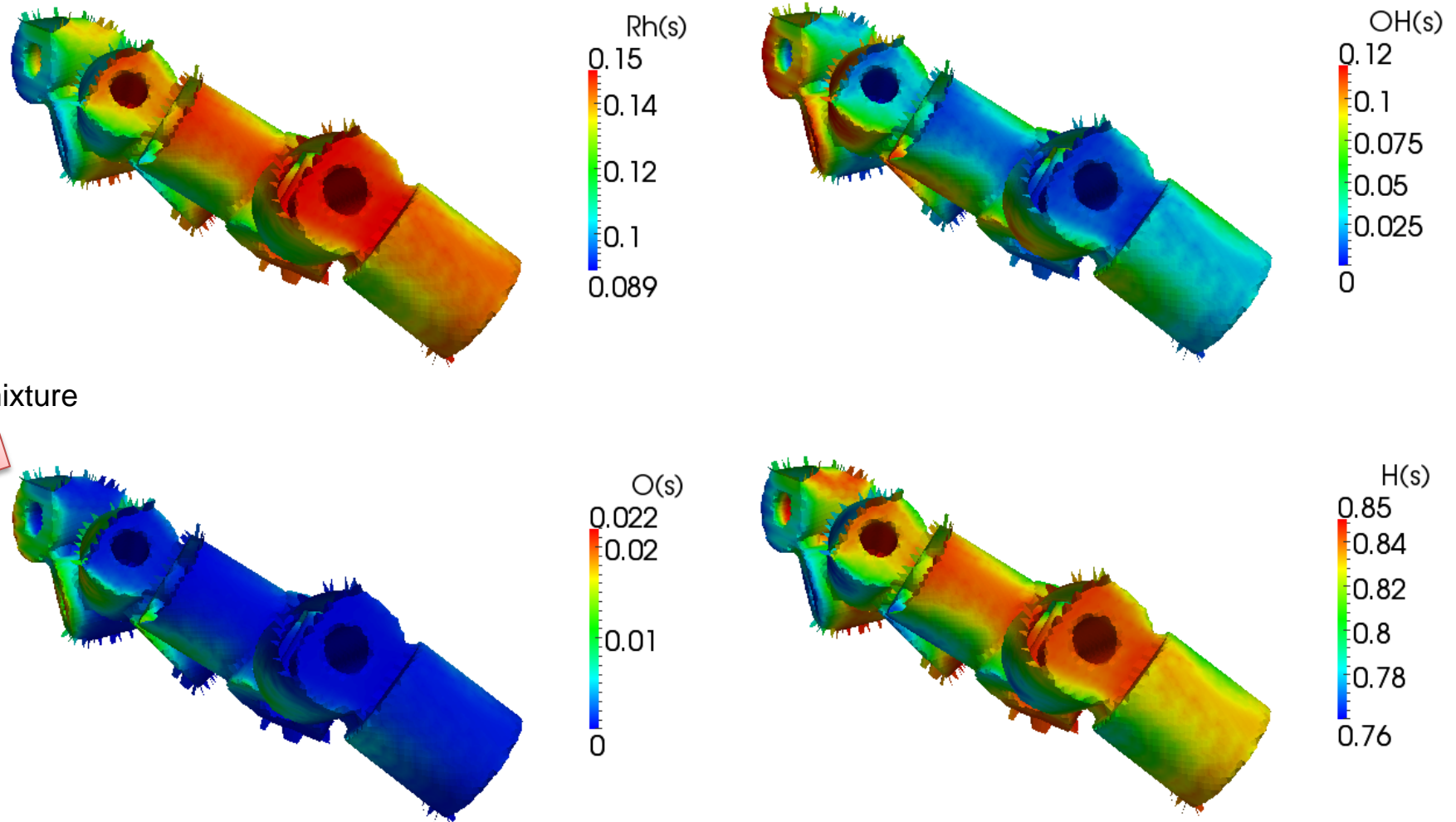
Gas-phase species

Inlet mixture



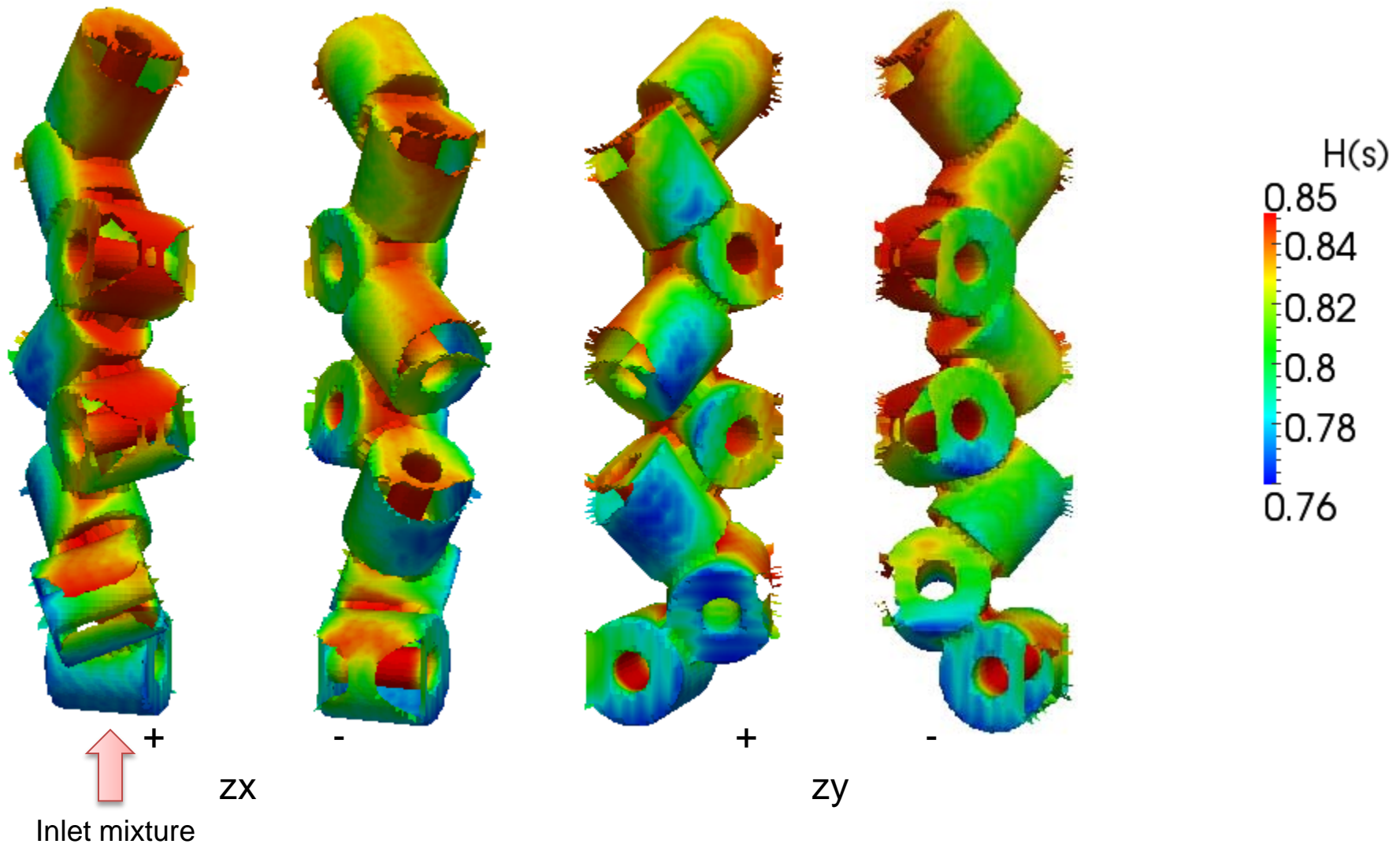
Show-case I: Rashig-ring bed

Adsorbed species at the catalyst surface



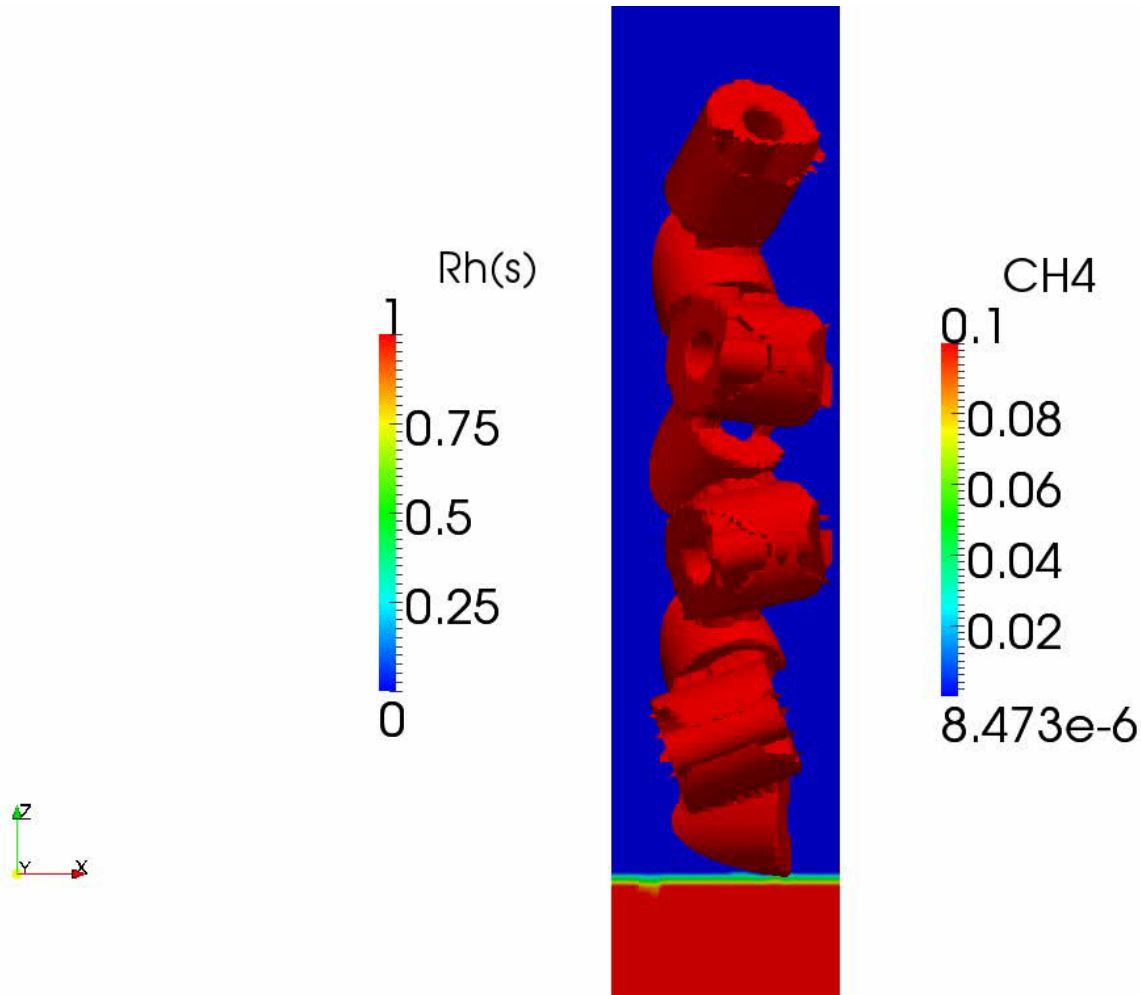
Show-case I: Rashig-ring bed

Adsorbed species at the catalyst surface



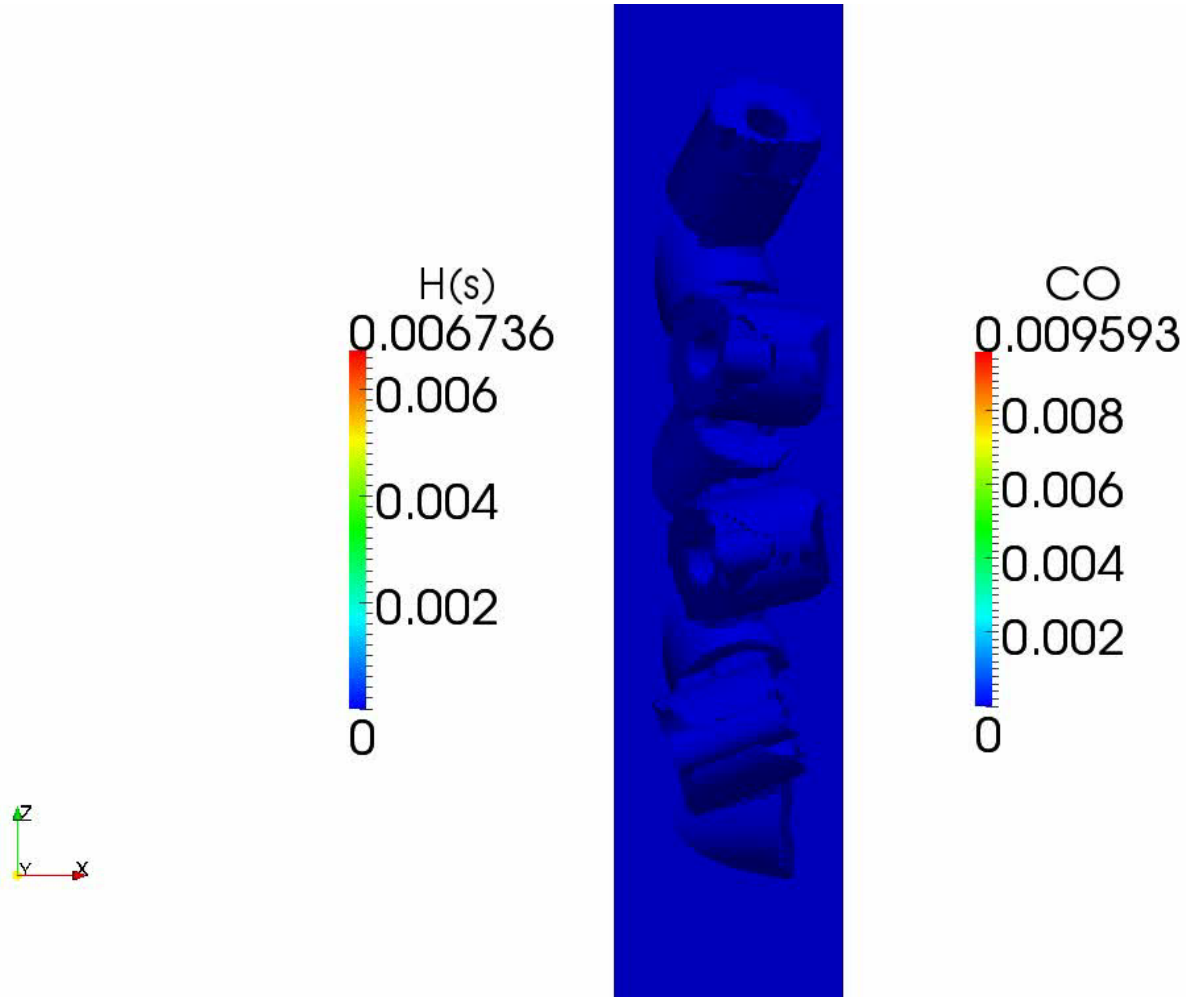
Show-case I: Rashig-ring bed

Dynamics of the system

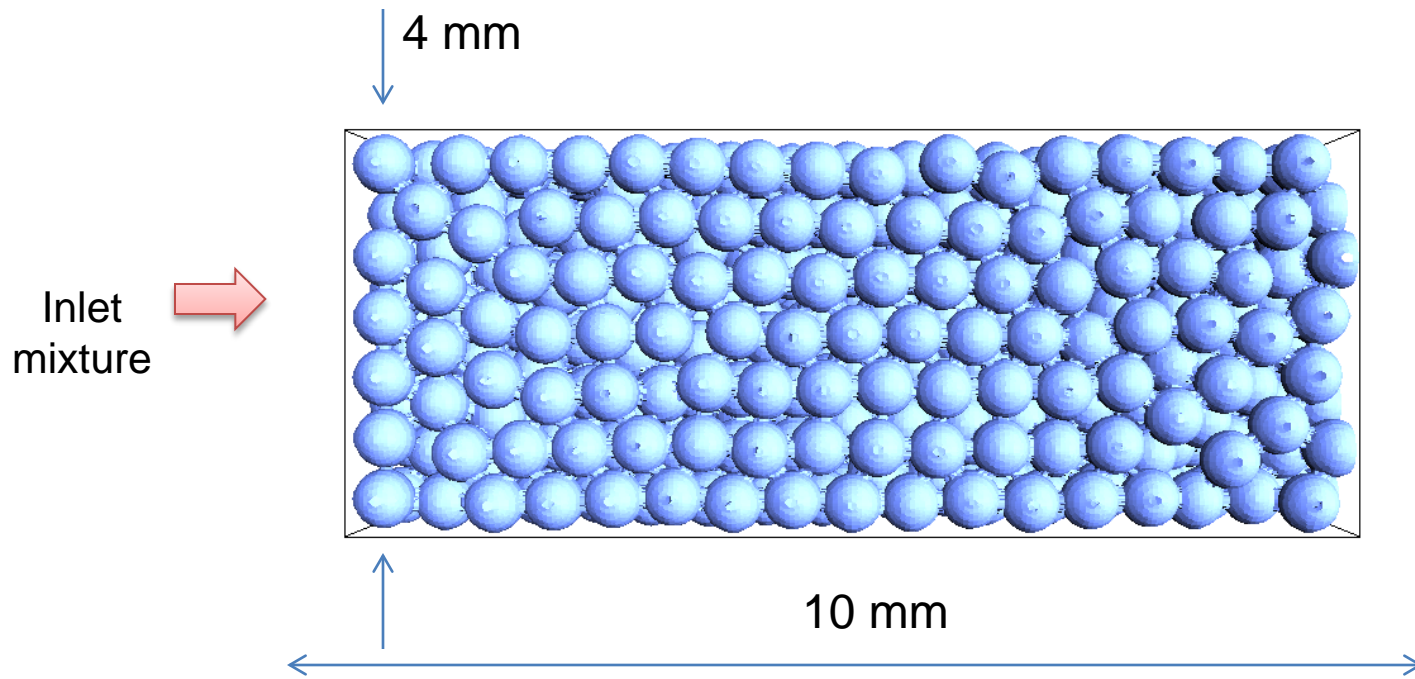


Show-case I: Rashig-ring bed

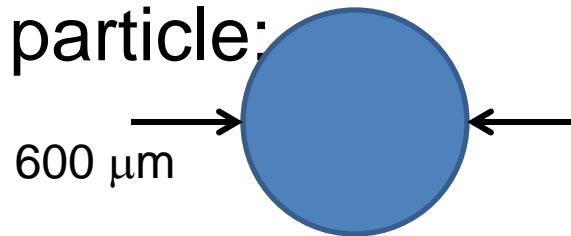
Dynamics of the system



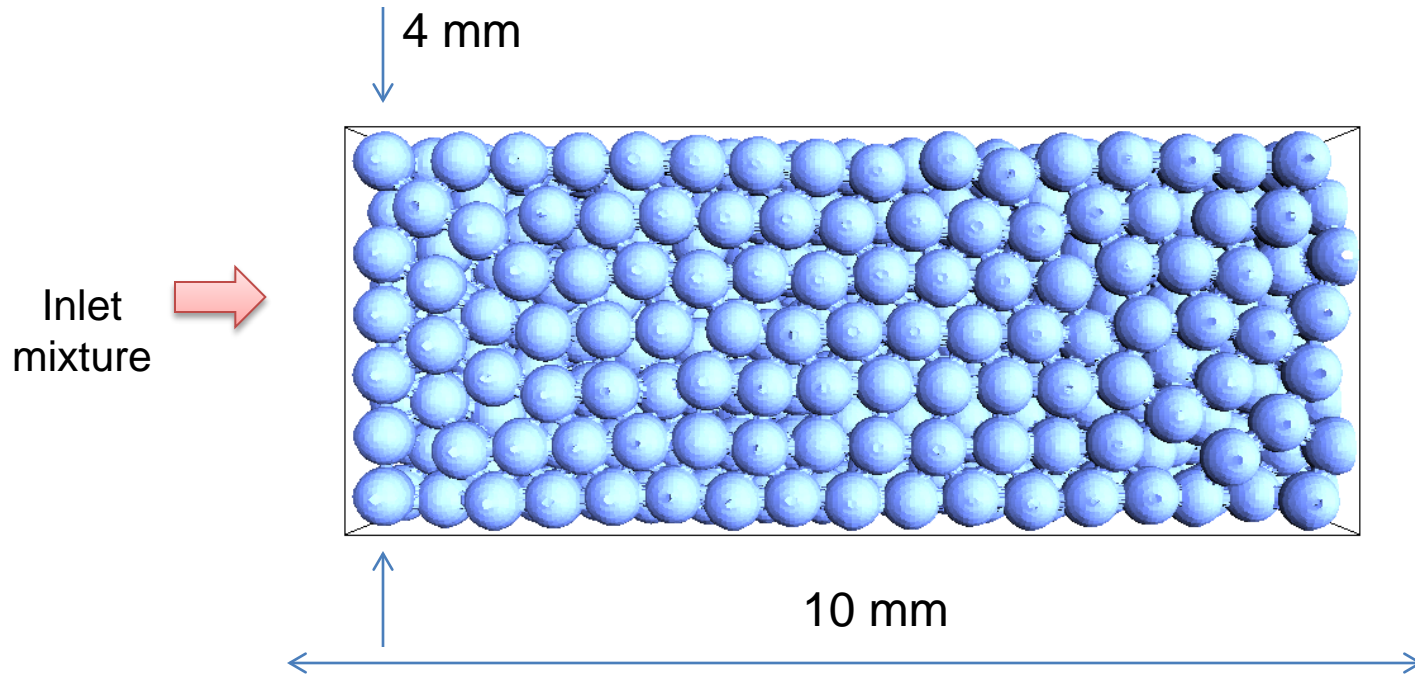
Show-case II: packed bed of spheres



Catalytic particle:



Show-case II: packed bed of spheres



3D Unstructured Mesh: ~2,000,000 cells

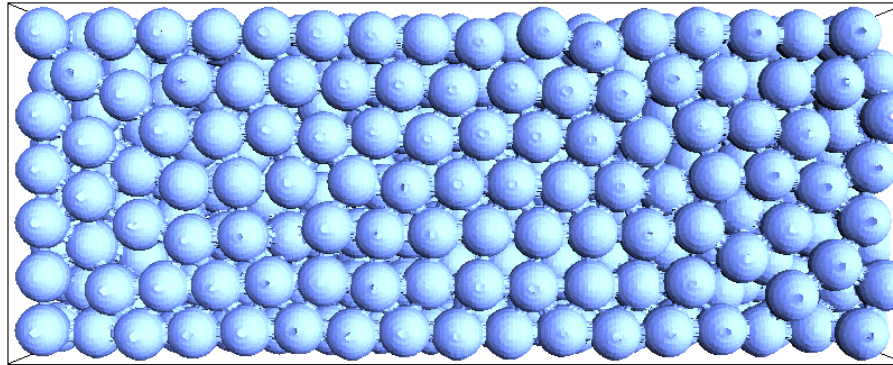
✓ Homogeneous reactors: ~1,000,000

✓ Heterogeneous reactors: ~1,000,000

Show-case II: packed bed of spheres

Laminar flow ($Re = 20$)

Inlet
mixture



C1 microkinetic model on Rh:

82 reaction steps

13 adsorbed species

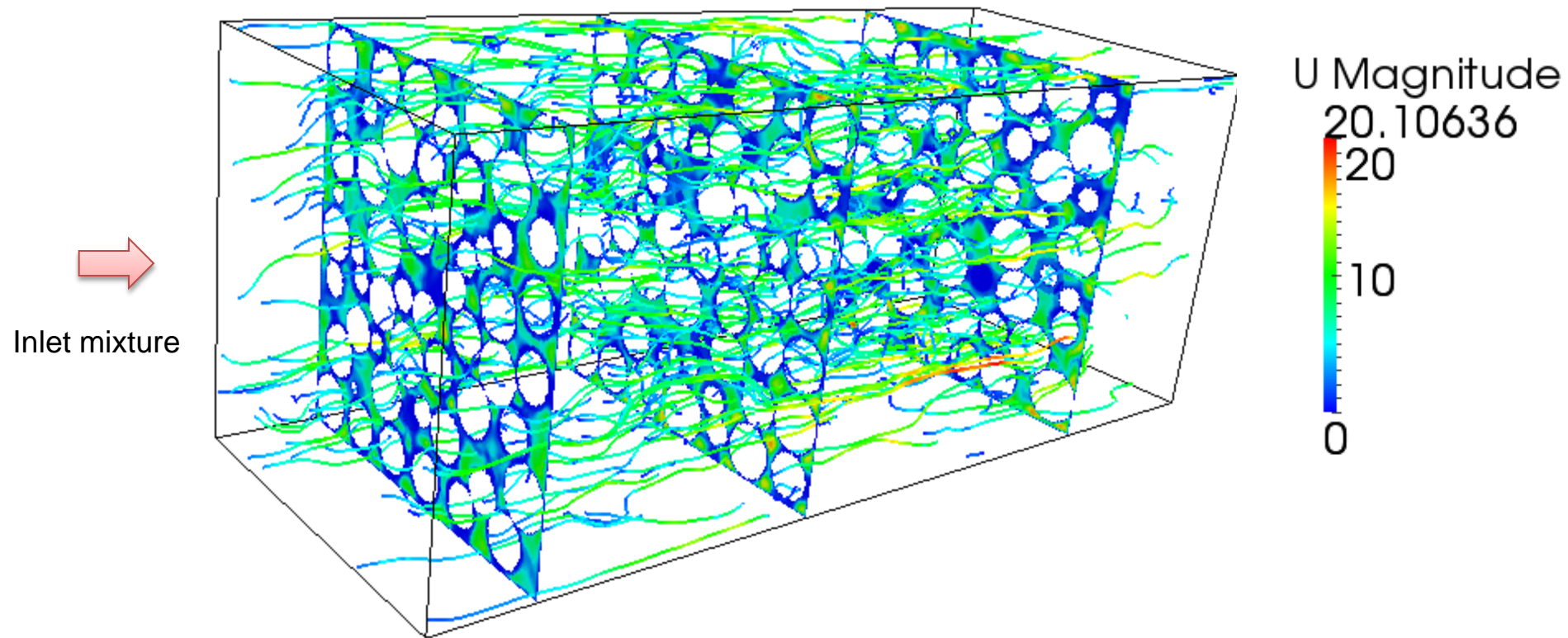
UBI-QEP and DFT refinement

M. Maestri et al., AIChE J., 2009

Operating conditions	
Inlet diameter	4 mm
Total length	10 mm
H ₂ mole fraction	0.036(-)
O ₂ mole fraction	0.014(-)
N ₂ mole fraction	0.95 (-)
Temperature	573 K
Inlet velocity	1.7 m/s

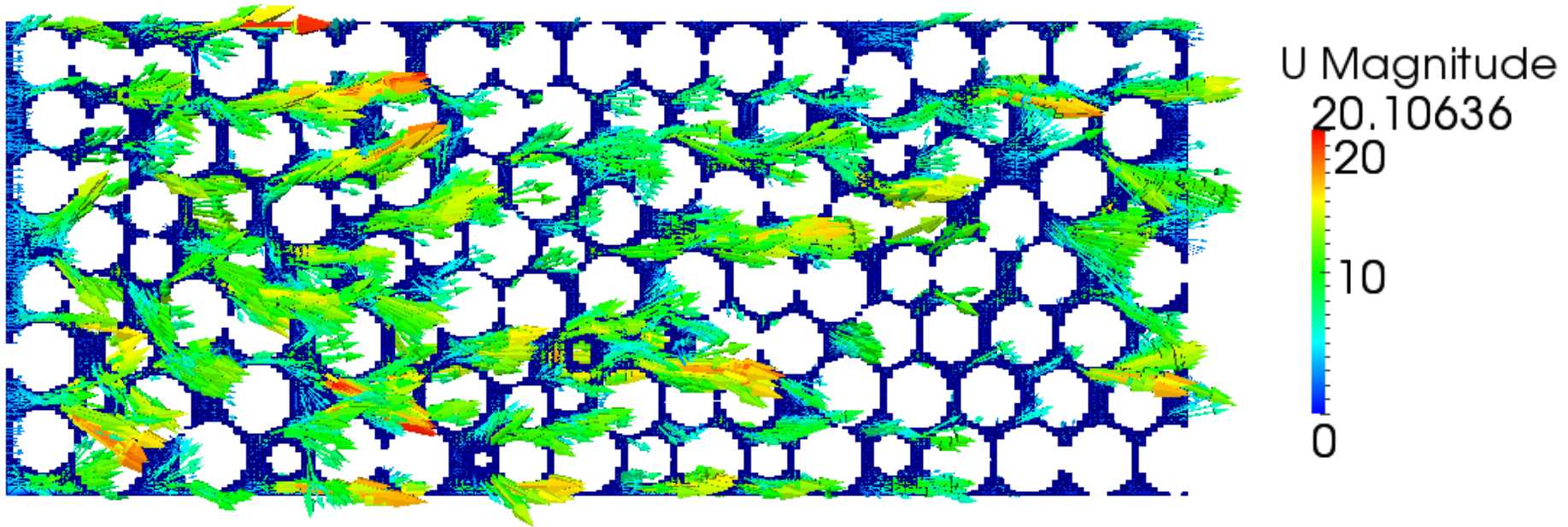
Show-case II: packed bed of spheres

Flow-field



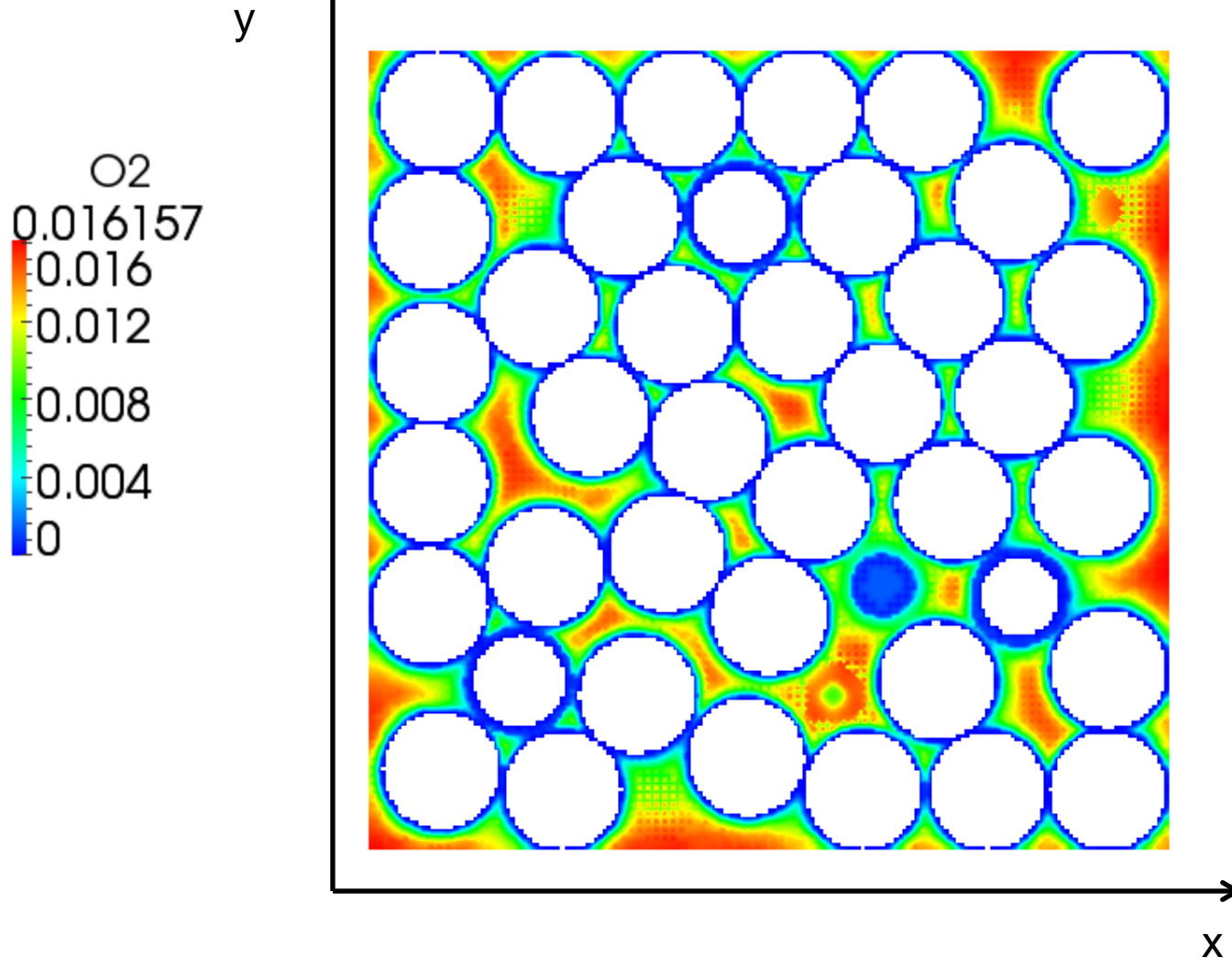
Show-case II: packed bed of spheres

Flow-field

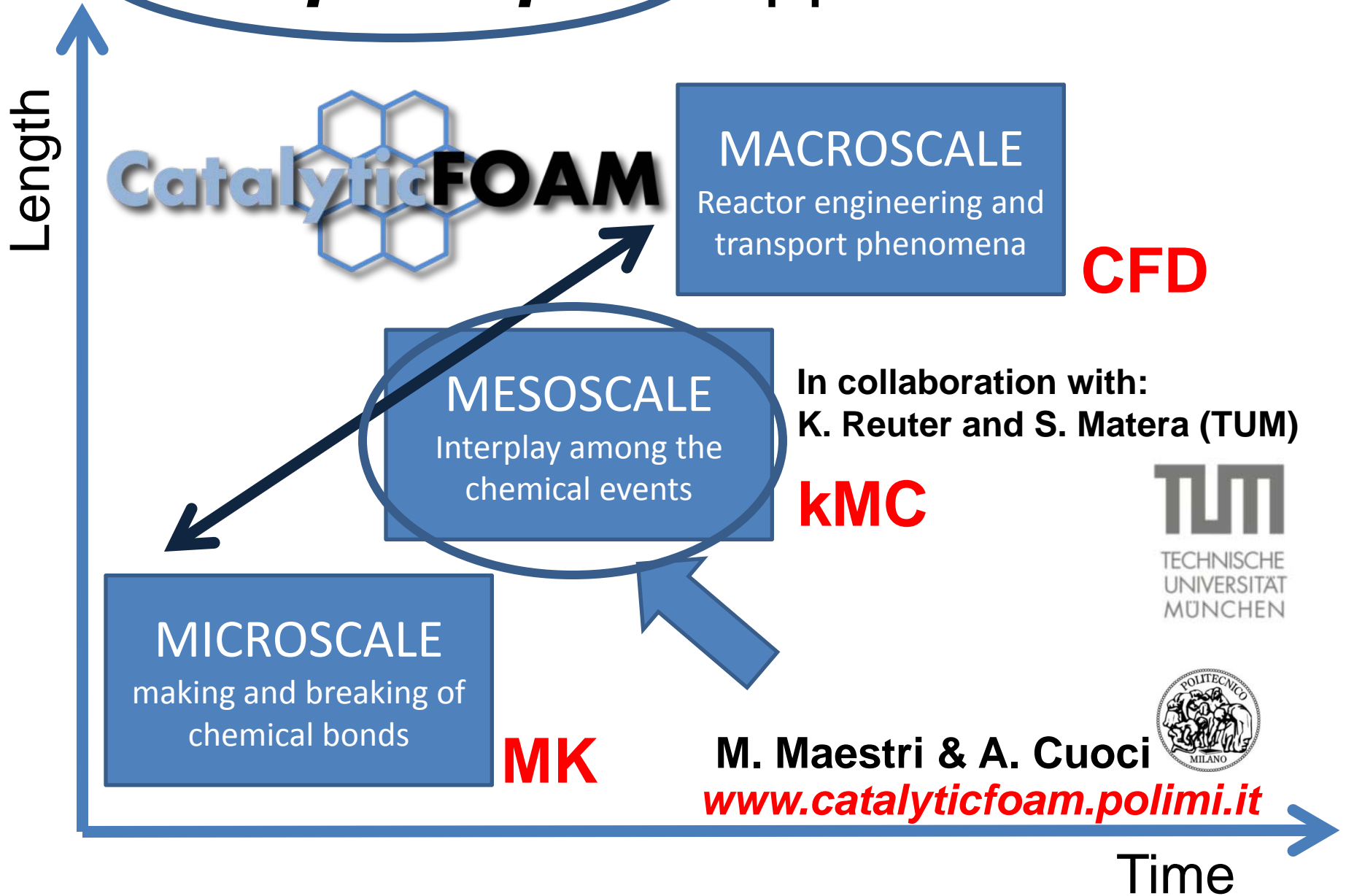


Show-case II: packed bed of spheres

Gas-phase species



A **“first-principles”** approach to CRE



First-principles kinetic Monte Carlo

- Evaluate the statistical interplay of large number of elementary processes
- open non-equilibrium system → need to explicitly follow the time evolution
- rare event dynamics → Molecular Dynamics simulations unsuitable. Map on a lattice model
→ Markov jump process description

$$\frac{d}{dt} P(\mathbf{x}, t) = \sum_y k(\mathbf{x}, y) P(\mathbf{y}, t) - \sum_y k(\mathbf{y}, \mathbf{x}) P(\mathbf{x}, t)$$

- Each site a has own entry in \mathbf{x} denoting its adsorbate state x_a
- Simulate trajectories $\mathbf{x}(t)$ (kinetic Monte Carlo)

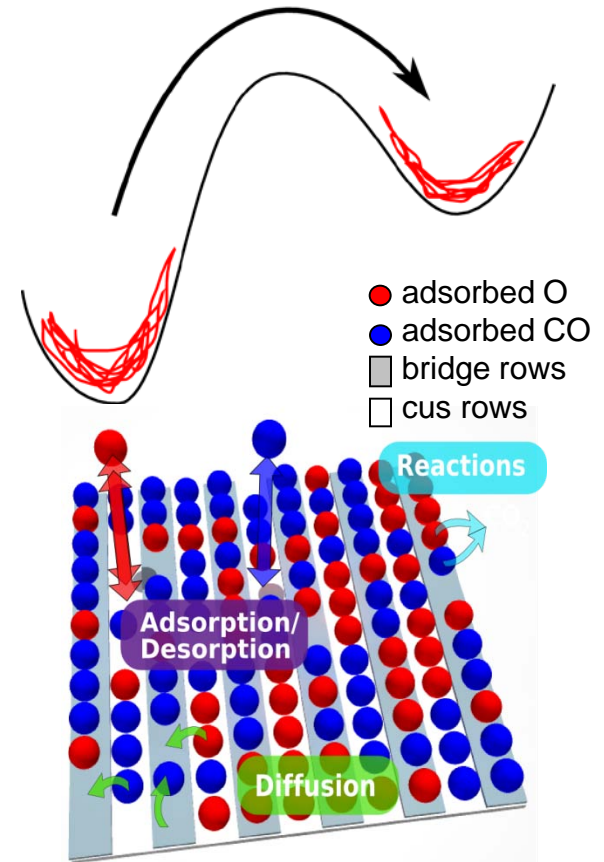


Image courtesy of Dr. S. Matera (TUM)

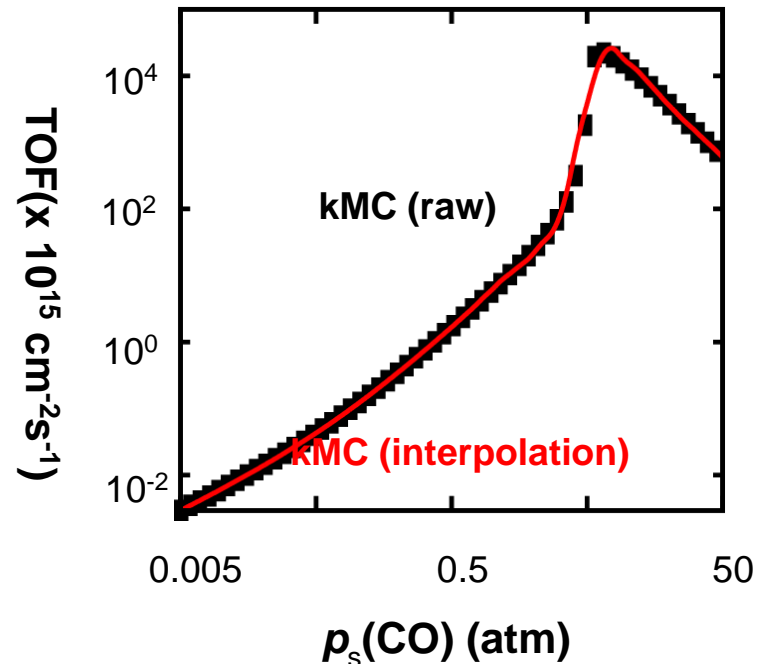
Linking the scales

- Continuum equations need boundary conditions for the mass fluxes j^α at the surface:

$$j_n^\alpha = v^\alpha M^\alpha \mathbf{TOF}$$

- Coupled problem:** to determine the TOF with 1p-kMC the pressures at the surface are needed, but the pressure field depends on the TOF
- kMC too expensive** for direct coupling to the flow solver
- Run kMC beforehand and interpolate (Modified Shepard)
- Very efficient
- Easily extendable to more complex geometries

$T_s = 600\text{K}, p_s(\text{O}_2) = 1\text{atm}$



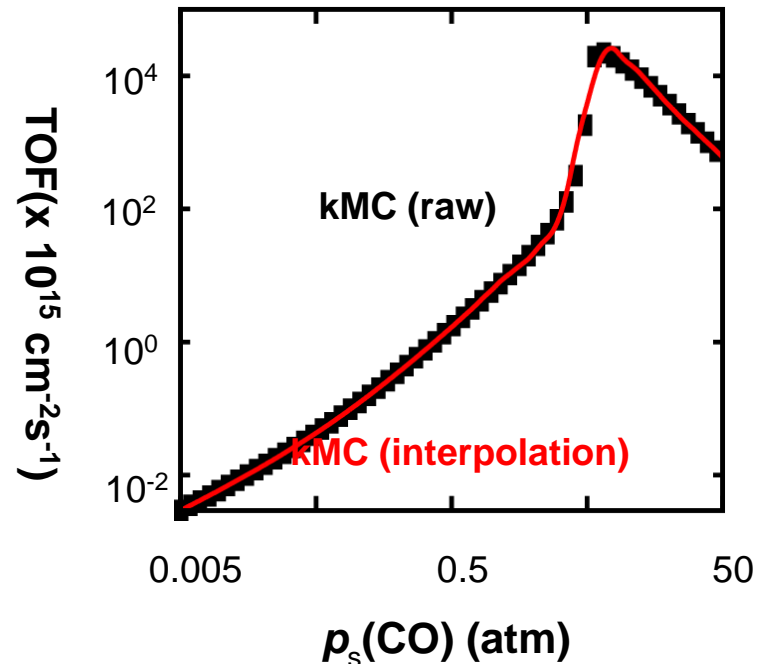
Linking the scales

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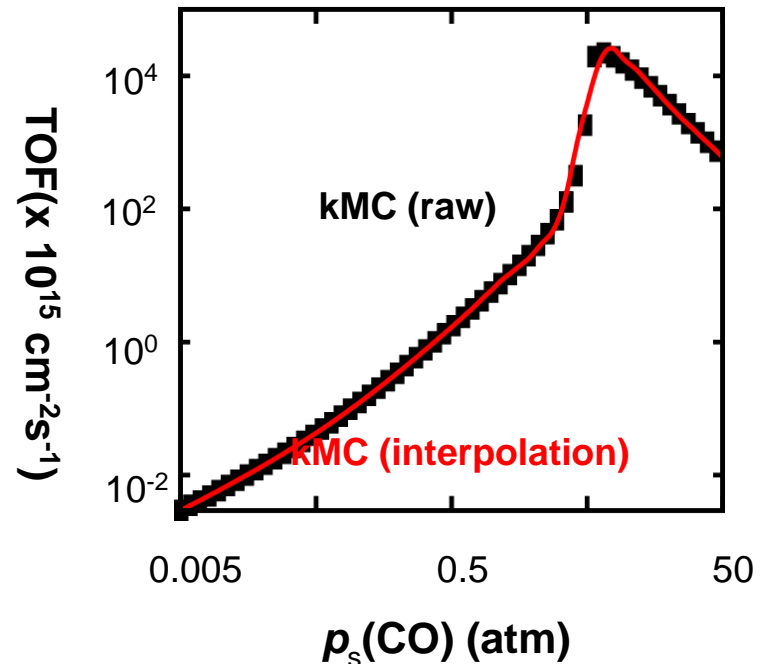
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$T_s = 600\text{K}, p_s(\text{O}_2) = 1\text{atm}$



Karsten's tutorial this afternoon

Show-case: the “reactor STM”

REVIEW OF SCIENTIFIC INSTRUMENTS

VOLUME 69, NUMBER 11

NOVEMBER 1998

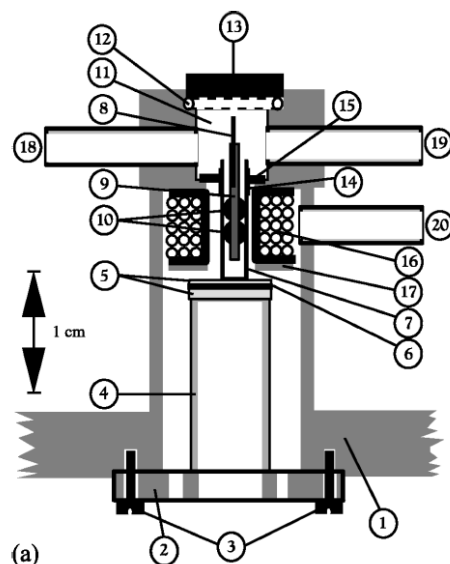
The “Reactor STM”: A scanning tunneling microscope for investigation of catalytic surfaces at semi-industrial reaction conditions

P. B. Rasmussen, B. L. M. Hendriksen,^{a)} H. Zeijlemaker, and H. G. Ficke
FOM-Institute for Atomic and Molecular Physics, Kruislaan 407, 1098 SJ Amsterdam, The Netherlands

J. W. M. Frenken
*Kamerlingh Onnes Laboratory, Leiden University, P.O. Box 9504, 2300 RA Leiden, The Netherlands
and FOM-Institute for Atomic and Molecular Physics, Kruislaan 407, 1098 SJ Amsterdam, The Netherlands*

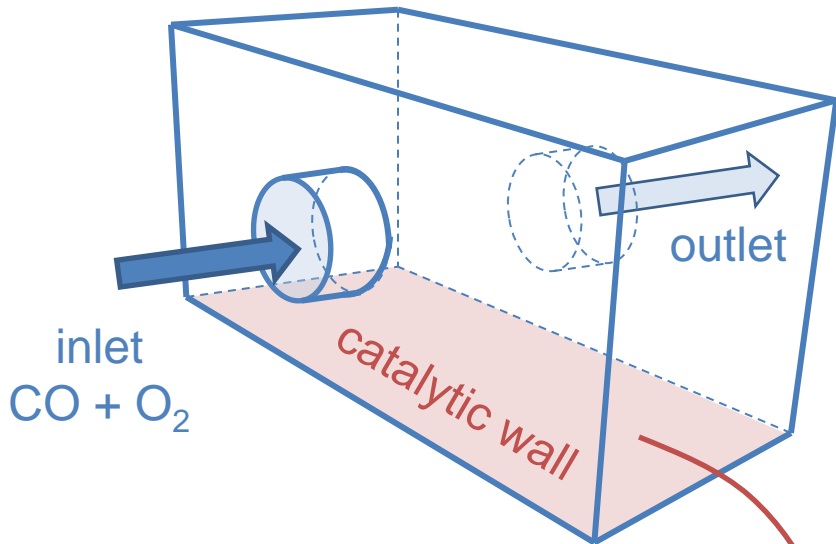
(Received 17 March 1998; accepted for publication 17 August 1998)

An instrument is introduced that combines a scanning tunneling microscope (STM) and a small volume (300 μ l) flow reactor, for the *in situ* study of catalytic surfaces at *semi-industrial* conditions.



Show-case: the “reactor STM”

Rasmussen et al., Review of scientific instrument, 69 (1998) 3879



Operating conditions

T: 600 K

P: 1 atm

Inlet: CO + O₂ (66%, 34% Vol)

Inlet velocity: 5 cm/s

Catalytic Wall
Catalyst: Ru₂O

CO oxidation on Ru₂O

- Rate constants $k(\mathbf{x}, \mathbf{y})$ from DFT and harmonic Transition State Theory
- Model system: CO oxidation on RuO₂(110)
 - 2 types of sites, bridge and cus

K. Reuter and M. Scheffler, *Phys. Rev. B* **73**, 045433 (2006)

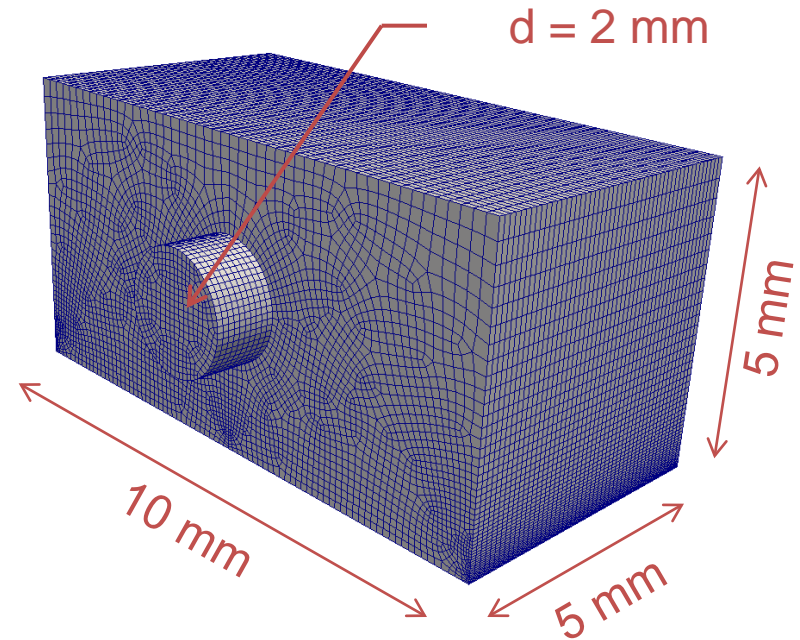
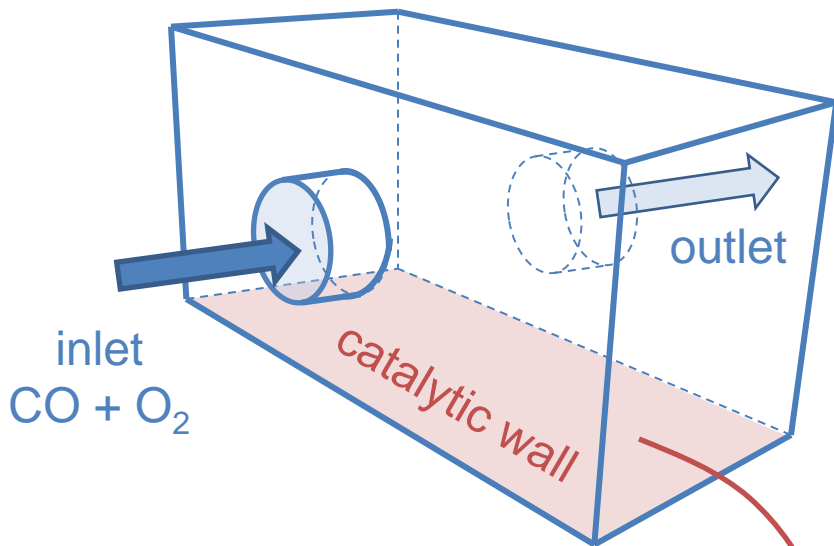


catalyticFOAM (interpolated kMC)

www.catalyticfoam.polimi.it

Show-case: the “reactor STM”

Rasmussen et al., Review of scientific instrument, 69 (1998) 3879

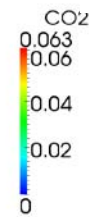
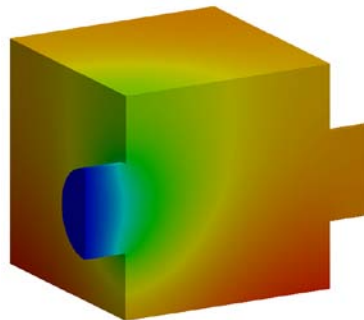
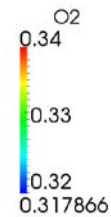
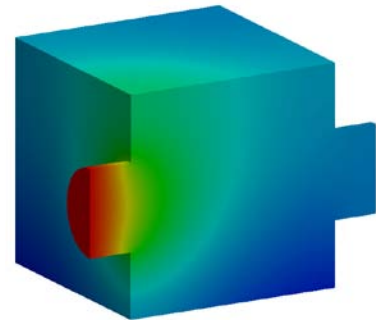
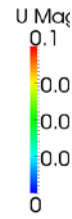
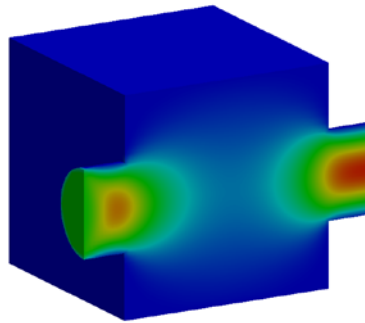
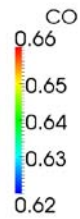
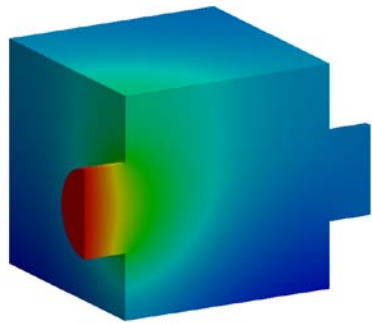


Operating conditions
T: 600 K
P: 1 atm
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Inlet velocity: 5 cm/s

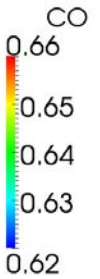
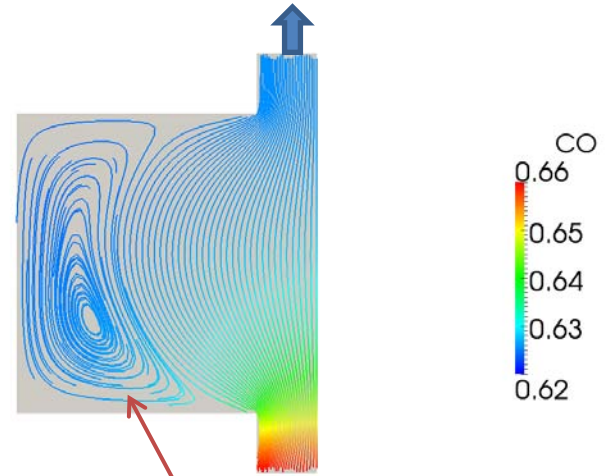
Catalytic Wall
Catalyst: Ru₂O

Computational details
Mesh: unstructured, ~90,000 cells
Discretization: 2nd order, centered
Max time step: 10⁻⁴ s
CPU time: ~2 s per time step

Results



Stream lines



Strong recirculations

**Catalytic Wall
Catalyst: Ru₂O**

Conclusions & perspectives

- ✓ Efficient coupling between heterogeneous microkinetic models and computational fluid dynamics (complex and fundamental chemistry with complex and general geometries)
- ✓ Description of the solid phase (diffusion/conduction and reaction within the solid: assessment of internal mass transfer limitation)
- ✓ Implementation of the interpolated kMC methodology in catalyticFOAM (in collaboration with K. Reuter/S. Matera, TUM)
- ✓ Multiscale framework for the first-principles analysis of catalytic processes



Highlights

CATALYTICFOAM ON CHEMICAL ENGINEERING SCIENCE

A recent publication on Chemical Engineering Science describes the CatalyticFOAM solver and shows several examples of applications to heterogeneous reacting systems.

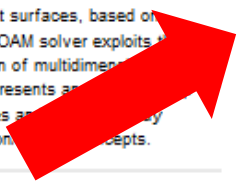
★ Disclaimer
catalyticFOAM is an academic initiative on the extension of OpenFOAM®.
In particular, it is neither approved nor endorsed by ESI Group, the producer of OpenFOAM® software and owner of the OpenFOAM® trademark.
You find the official web-site of the OpenFOAM® foundation at www.openfoam.org

📄 Workshop on HPC

Welcome to CatalyticFOAM

We have developed a new solver for OpenFOAM, that allows for the solution of Navier-Stokes equations for complex and general geometries for reacting flows at surfaces, based on microkinetic descriptions of the surface reactivity. The CatalyticFOAM solver exploits an operator-splitting technique in order to make possible the simulation of multidimensional systems with complex kinetic mechanisms. Such an approach represents an important step towards the rational understanding and development of new reaction concepts.

[Detailed kinetics for homogeneous and heterogeneous](#)



📄 Download the Code

CatalyticFOAM is distributed for **free** and it is fully compatible with the most recent version of OpenFOAM 2.x.
[Click here to download the code.](#)

👤 Join the catalyticFOAM team!

Are you interested in joining the CatalyticFOAM team for your thesis or post-graduate research? [Click here!](#)

Acknowledgements



Catalytic  **FOAM @polimi.it**

M. Maestri & A. Cuoci

**Tiziano Maffei, G. Gentile, F. Manelli, S. Rebughini,
S. Goisis, A. Osio, M. Calonaci, F. Furnari, B. Baran, Y. Niyazi**



Alexander von Humboldt
Stiftung / Foundation



Laboratory
of Catalysis and
Catalytic Processes | **LCCP**



Thank you for your attention!

Politecnico di Milano

Raffaello, The school of Athens, 1509, Apostolic Palace, Roma

www.catalyticfoam.polimi.it



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