

Dissipative Particle Dynamics Simulations with Chemical Reactions: Application to Thermal Decomposition of RDX

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CECAM 2013
September 8-13, 2013
Platja d'Aro, Spain

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Czech Science Foundation,
project no. 13-02938S

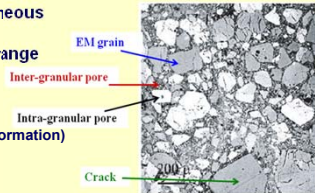
Objective

- Develop capability to simulate the response of materials to mechanical and thermal stimuli at the micro- and mesoscale¹

Motivation

- Nanocomposites are inherently heterogeneous

- Stimuli can incite responses over a wide range of spatial and temporal scales



- Known responses include:
 - Structural rearrangements (e.g., plastic deformation)
 - Phase transitions
 - Chemical reactions

Coarse-Grain Models

Top-Down CGing

Build CG model by:

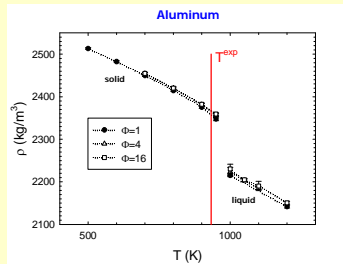
- Choosing an analytical description of the CG interactions
- Fitting the CG interaction parameters to observables (experimental or simulation)

Example: Aluminum

- Pair-wise, density-dependent potential^{2,3}

$$U_{SC} = \sum_i \sum_{j \neq i} \left[\frac{r_{ij}}{r_{ij}^n} \right] - \sum_i C_i \varepsilon_{ij} \sqrt{\sum_{j \neq i} \left[\frac{r_{ij}}{r_{ij}^m} \right]}$$

long-range, attraction short-range, cohesion



Phi: level of coarse-graining

- Fit parameters to 0 K properties (lattice constant, cohesive energy, bulk modulus)
- Re-fit to melting temperature using constant-pressure DPD (DPD-P)

- Scale to higher CG levels by fixing:⁴
 - number density
 - energy per particle

$$r_0^3 = \Phi^{1/3} r_0$$

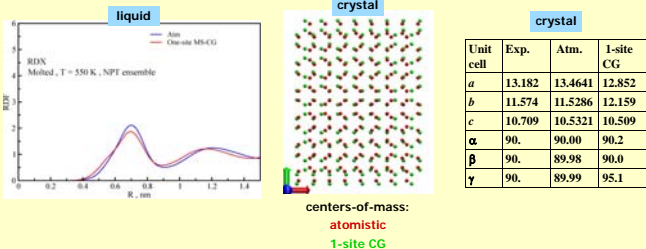
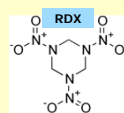
Bottom-Up CGing

Multiscale Coarse-Grain method (MSCG):

- Force matching approach
- Develop pairwise potentials directly from atomistic simulations

Example: RDX

- One-site model matched to disordered solid (350 K) and liquid (550 K)



centers-of-mass:
atomistic
1-site CG

Methods

Constant-Energy Dissipative Particle Dynamics^{6,7} (DPD-E)

- Variant of standard Dissipative Particle Dynamics (DPD)
- Both momentum and energy conserved in DPD-E
- Internal energy variable assigned to each particle, u_i

Equations of motion:

$$\frac{d\mathbf{r}_i}{dt} = \mathbf{v}_i(t)$$

position

$$m_i \frac{d\mathbf{v}_i}{dt} = \mathbf{f}_i(t) = \sum_{j \neq i} (\mathbf{F}_{ij}^C + \mathbf{F}_{ij}^D + \mathbf{F}_{ij}^R)$$

velocity

$$\frac{du_i}{dt} = \frac{du_i^{mech}}{dt} + \frac{du_i^{cond}}{dt}$$

internal energy

particles exchange kinetic & internal energy

- Each particle assigned u_i, s_i and θ_i

- Need mesoparticle equation-of-state that governs thermodynamics of implicit d.o.f.

- KE lost/gained by dissipative and random interactions absorbed/released by u_i

Mesoparticle EOS: $u_i = u_i(\theta_i)$

Classical Limit: $C_{v,i} = (3n - 3)k_B = \text{const}$ ($n = \#$ of CG DOF)

$$u_i = C_{v,i} \theta_i$$

Based on Thermochemical Data:

$$u_i = \frac{\Delta H_{f,i}(T_r)}{N_A} + \int_{T_r}^T C_{p,i}(T) dT - \frac{5}{2} k_B \theta_i$$

Fluctuation-Dissipation Theorems

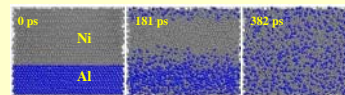
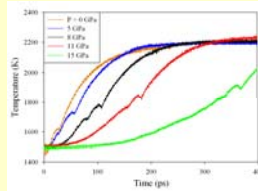
$$\gamma_{ij} = \frac{\sigma_{ij}^2}{2k_B} \left(\frac{1}{\theta_i} + \frac{1}{\theta_j} \right) \quad \alpha_{ij}^2 = 2k_B \kappa_{ij}$$

Parameterize $C_v = C_v(\theta)$ data

Possible to include quantum effects from first principles simulation data

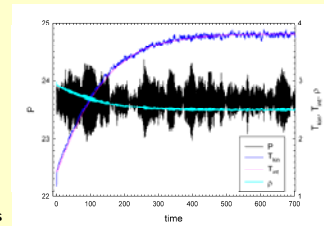
Constant-Enthalpy Dissipative Particle Dynamics¹ (DPD-H)

molecular dynamics simulations of Ni/Al alloying⁸



pressure strongly influences rate of alloying

Constant-Enthalpy Method Needed



- Combine DPD-P with DPD-E
- Add either Hoover or Langevin barostat EOM to DPD-E EOM
- Langevin barostat requires "barostat temperature" parameter

Example:

DPD model fluid

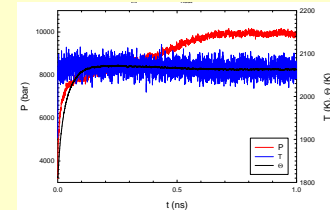
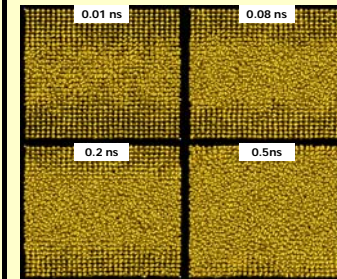
- > 1/3 of the particles heated at $t=0$

Formulated efficient numerical integration algorithms for DPD variants!
required for models of interest improved conservation of quantities

Applications

THERMAL IMPULSE

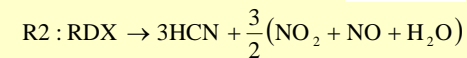
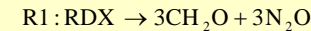
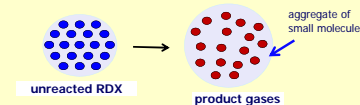
- CG Ni initially at 1300 K
- interior slab heated to 3000 K



Extension: Chemical Reactions (DPD-RX-E)

- Mesoparticles act as 'microreactors'⁹
- Concentration changes w/i mesoparticles governed by rate eqns.
- Interaction potential depends on concentration: $U_{ij}^C = U_{ij}^C(r_{ij}, [i], [j])$

Ex: RDX decomposition¹⁰



Rate Equations:

$$\frac{d[\text{RDX}]}{dt} = -k_{R1}[\text{RDX}] - k_{R2}[\text{RDX}]$$

$$\frac{d[\text{CH}_2\text{O}]}{dt} = 3k_{R1}[\text{RDX}]$$

$$\frac{d[\text{NO}_2]}{dt} = \frac{3}{2}k_{R2}[\text{RDX}]$$

$$\frac{d[\text{N}_2\text{O}]}{dt} = 3k_{R1}[\text{RDX}]$$

$$\frac{d[\text{HCN}]}{dt} = 3k_{R2}[\text{RDX}]$$

$$\frac{d[\text{NO}]}{dt} = \frac{3}{2}k_{R2}[\text{RDX}]$$

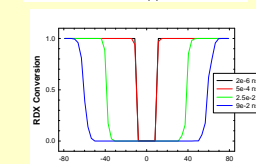
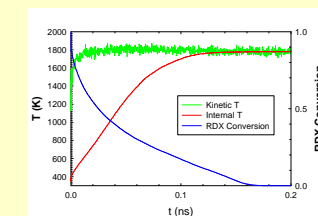
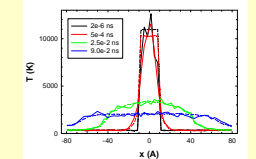
$$\frac{d[\text{H}_2\text{O}]}{dt} = \frac{3}{2}k_{R2}[\text{RDX}]$$

$$k_{Rj} = A_{Rj} \exp\left(-\frac{E_{Rj}}{k_B \theta}\right)$$

depending on internal temperature

Reaction	A (s ⁻¹)	E (kJ mol ⁻¹)
R1	6.02 x 10 ¹³	150.624
R2	2.51 x 10 ¹⁶	184.096

Thermal Impulse: pure RDX initially at 350 K ⇒ 20 Å slab heated to 10000 K



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⁷Maillet, Souldard, and Stoltz, *Europhys. Lett.*, 78, 68001 (2007)

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